NAVAL POSTGRADUATE SCHOOL MONTEREY, CALIFORNIA



THESIS



ESTIMATE OF MAXIMUM DETECTION RANGE FOR FLIR FROM EOMET 95 MEASUREMENT DATA

by

Chih-Li Yu

December 1997

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ESTIMATE OF MAXIMUM DETECTION RANGE FOR FLIR FROM EOMET 95 MEASUREMENT DATA

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Submitted in partial fulfillment of the requirements for the degree of

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ABSTRACT

FLIR sensor maximum range predictions for operational use may be based on the intersection of apparent target contrast temperature difference (ΔT_{app}) and sensor minimum resolvable (MRTD) or minimum detectable temperature difference (MDTD), each expressed as a function of range. Ranges obtained using the SEARAD code (MODTRAN modified for sea surface radiance) are compared with those based on Beer's Law with constant extinction coefficient. Physical and meteorological parameters for the common scenario were taken from the database of the EOMET95 measurements in Monterey Bay, with the research vessel POINT SUR as instrumented target and measurement platform. MRTD and MDTD functions were developed as functions of range for a generic Common Module FLIR using the Johnson Criterion for resolution with a parallelepiped geometry model of the POINT SUR. The Beer's Law results underestimate the SEARAD-based ranges by approximately 50% for detection but less for classification and identification. Replacement of Beer's Law with MODTRANcomputed transmittance reduces this discrepancy. SEARAD-based modeled sea radiance and short range contrast temperature show unexpected variation with range.

TABLE OF CONTENTS

I. INTRODUCTION1
II. INFRARED RADIATION FUNDAMENTALS3
A. THEORY OF BLACKBODY RADIATION3
1. Planck's Radiation Law4
2. Emissivity4
3. Stefan-Boltzmann Law5
4. Kirchhoff's Law6
5. Lambert-Beer Law6
B. INFRARED RADIATION SOURCES6
C. ATMOSPHERIC PROPAGATION OF INFRARED RADIATION7
1. Absorption Effects7
2. Scattering Effects8
a. Rayleigh Scattering9
b. Mie Scattering10
III. EOMET95 EXPERIMENT AND DATA COLLECTION11
A. INTRODUCTION11
B. DATA MEASUREMENTS12
1. Imaging System12
2. Calibration Technique12
3. Target Temperature12
4 Visual Imaging13
IV. MRTD AND MDTD15
A. MINIMUM RESOLVABLE TEMPERATURE DIFFERENCE15

	B. MINIMUM DETECTABLE TEMPERATURE DIFFERENCE	17
	C. MRTD AND MDTD COMPUTATION	17
V.	DATA COMPUTATIONS AND ANALYSIS	19
	A. APPARENT ΔT COMPUTATION	19
	1. Data Summary of Infrared Measurements in EOMET95	19
	2 Ship Temperature Computation	20
	3. Ship GPS Position and Heading Data Correlation	21
	4. Temperature and Radiance Conversion	22
	5. Transmittance and Path Radiance	23
	B. MRTD AND MDTD VS RANGE COMPUTATION	24
	1. Range, Elevation and Azimuth Angle	24
	a. Condition 1	25
	b. Condition 2	25
	2. Projected Area of the Ship A _t	26
	3. Critical Dimension D _c	26
•	4. Conversion of Spatial Frequency to Range	28
VI	DATA ANALYSIS AND CONCLUSIONS	29
	A. APPARENT ΔT BY ATTENUATION OF SOURCE ΔT	30
	B. RADIANCE COMPUTATION METHOD	30
	C. SEARAD	31
	D. DISCUSSION OF THE DATA AND CONCLUSIONS	32
APP	PENDIX A. THERMISTOR SAMPLE OUTPUT FILE	65
APP	PENDIX B. PROPORTIONAL RADIATION TABLE	67

APPENDIX C. LOOK-UP TABLE	69
APPENDIX D. AUXILIARY PROGRAM (SEARAD CODE)	
A. INTRODUCTION	75
B. UNZIP SEARAD (INSTALLATION)	75
C. SEARAD SAMPLE DESCRIPTION	76
D. SEARAD MODEL	77
APPENDIX E. DESCRIPTION OF EACH CARD IN SEARAD INPUT FILE	79
APPENDIX F. SEARAD INPUT DATA FILE	83
APPENDIX G. SEARAD OUTPUT DATA FILE	87
APPENDIX H. GPS DATA FILE	95
APPENDIX I. RADIOSONDE METEOROLOGICAL DATA FILE	115
APPENDIX J. MATLAB CODE FOR COMPUTATION	137
A. GPS, ELEVATION AND AZIMUTH ANGLE CALCULATION	137
B. MRTD AND MDTD VS SPATIAL FREQUENCY	139
C. MRTD AND MDTD AND ΔT VS RANGE FOR DETECTION	140
D.MRTD AND ΔT VS RANGE FOR CLASSIFICATION	142
E. MRTD AND ΔT VS RANGE FOR IDENTIFICATION	144
LIST OF REFERENCES	1.47

INITIAL DISTRIBUTION LIST	.14	49
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I. INTRODUCTION

Electro-optical and infrared sensors detect and identify targets by discrimination of their thermal contrast against the cluttered background. In the case of targets at sea, this means distinguishing the target radiance from the sea or sky background radiance, attenuated by transmission through the atmosphere, together with the radiance emitted by the atmosphere along the path. The performance of electro-optical sensors is greatly influenced by atmospheric factors related to the marine boundary layer and the scenario geometry. Polarized images of the research vessel POINT SUR (R/V POINT SUR) and of the Netherlands Oceanographic ship HM Tydeman have shown that use of a polarizer can improve contrast temperature difference ΔT against background.[Ref.1] What action is still needed is a comparison of predicted detection range with polarization and without polarization to see if the increased contrast increases the detection/ recognition range more than the loss of energy (photons) decreases it.

This thesis addresses the prediction of the detection/recognition range without polarization. The concept of the approach is that at the maximum detection/recognition range the projected apparent target background temperature difference (ΔT_{app}) must equal the apparent contrast temperature difference required by the sensor. The sensor performance is described by the parameter Minimum Detectable Temperature Difference (MDTD) or Minimum Resolvable Temperature Difference (MRTD) as appropriate. The apparent temperature contrast ΔT available at given range is computed from the zero range target temperature converted to apparent blackbody radiance, and background radiance computed using the SEARAD[Ref. 2] atmospheric propagation code, a modified form of the standard MODTRAN code. SEARAD was also used to adjust the radiance for atmospheric attenuation and path radiance. SEARAD is a DOS-compatible program developed at NCCOSC-NRaD (Naval Command, Control and Ocean Surveillance Center-Naval Research and Development) for application to naval problems.

The source of meteorological parameters for the predictions was based on the EOMET95 experiment that was conducted on May 15 to 24, 1995 in which polarized image data was recorded from Monterey Bay Aquarium Research Institute at Moss Landing, CA. The Research Vessel POINT SUR (R/V POINT SUR) was used as a target and as a measurement platform. The ship skin temperature distribution was recorded every 20 seconds throughout the experiment using a set of 15 thermistors on the ship skin. Meteorological and sea surface data measured on board the POINT SUR were used as input to the atmospheric propagation computations. The meteorological parameters and observation range selected in this experiment were used as inputs to the "SEARAD" code to calculate the atmospheric infrared (8 to 12 µm) transmittance and path radiance.

After accessing the transmittance and path radiance calculated from SEARAD, Planck's radiation law was applied to find the apparent radiance difference and corresponding temperature difference (ΔT) at the detection range. Generic common module FLIR parameters tabulated by Shumaker, Wood and Thacker [Ref. 3:p. 8-59] were used to estimate MDTD/MRTD appropriate to a generic "Marine Patrol Aircraft" FLIR sensor, and the conventional Johnsion criterion used to deduce the equivalent operational target spatial frequency.

In selecting the scenario for this analysis the ship location, heading and aspect with respect to the polarizing images in the EOMET95 image data base were collated and processed; the collated data are listed in Appendix H and Appendix I to this thesis, for later analysis. After a brief summary of the relevant radiation propagation theory, the EOMET95 experimental procedure and measurement are discussed, including the procedure for target aspect and apparent dimensions, and the computation and modeling of the FLIR, MRTD, and MDTD functions are described. Computation of target contrast and MRTD and MDTD range estimates are then described, for selected target-sensor scenarios from the EOMET95 data base and followed with discussion of the results.

II. INFRARED RADIATION FUNDAMENTALS

Optical radiation covers the ultraviolet (UV), visible, and infrared (IR) portions of the electromagnetic spectrum. The ultraviolet portion ranges from about 0.1 to 0.38 μm . The visible portion is from approximately 0.38 to 0.76 µm in wavelength. The infrared portion is divided into the near infrared or short-wavelength infrared (SWIR) region (from 0.77 to 3 µm), the middle-wavelength infrared (MWIR) region (from 3 to 8 µm), the long-wavelength infrared (LWIR) region (from 8-14 μm), and the far and extreme infrared region (from 14 to 1000 µm). The radiant energy received by an optical system from a scene object can be generally broken down into two components: (1) radiant energy due to the self-emission of the object and (2) radiant energy reflected by the object due to external radiation sources. The objects being observed by the optical system can be categorized as either the target or the background. [Ref. 4:p. 37] The radiation emitted and reflected from the target and the background traverse through the atmospheric medium, where absorption and scattering take place by molecular constituents of the atmosphere and the aerosol particles suspended in it. Re-emission and scattering from these atmospheric components also contribute path radiance to the received power. The absorption, scattering, and emission are conventionally computed using standard DOD propagation computer codes. For this study the developmental SEARAD code was used. SEARAD is described further in Appendix D.

A. THEORY OF BLACKBODY RADIATION

This section summarizes commonly known material which can be found in many tutorial sources, for example "The Infrared Handbook" [Ref. 5]. All objects with a temperature above absolute zero emit radiation. Relative spectral intensity of the radiation is dependent primarily on the temperature of the object and on the radiant properties of the material the object is made of (in particular, the spectral emissivity of the

material). [Ref. 6:p. 24] A blackbody is defined as an ideal body or surface that absorbs all radiant energy incident upon it at any wavelength and at any angle of incidence, so that none of the radiant energy is reflected or transmitted. Therefore, the term blackbody refers to a perfect absorber of radiation. Because all radiant energy is absorbed by a blackbody and none is reflected or transmitted, it will appear to be "black". [Ref. 4:p. 44]

1. Planck's Radiation Law

Planck's radiation law can be used to calculate the spectral radiance of a blackbody source. Planck's equation satisfies thermodynamic requirements and gives the spectral radiant exitance $M_{bb}(\nu,T)$ of a blackbody in terms of temperature, T, and radiation frequency, ν :

$$M_{BB}(v,T) = \frac{2\pi h v^5}{c^3 (e^{hv/kT} - 1)}$$
, 2.1

where

h is Planck's constant,

c is the speed of light,

k is Boltzmann's constant (1.38054×10⁻²³ J-K⁻¹)

This equation can also be written in terms of wavelength, λ :

$$M_{BB}(\lambda,T) = \frac{2\pi hc^2}{\lambda^5 (e^{hc/\lambda kT} - 1)} , \qquad 2.2$$

Equation 2.1 and 2.2 express the spectral radiant exitance of a source radiating in a vacuum. For any other media, c should be replaced by the light velocity in the media, c/n, where n is the refractive index of that medium.

2. Emissivity

The radiation from all bodies in a wavelength range under consideration is dependent firstly on the temperature and secondly, in the case of non-black bodies, on the material composition and surface condition. The ratio of the emitted radiation of any given temperature radiator to the emitted radiation of a black body of the same temperature is known as the emissivity.[Ref. 6:p. 50]

$$M=\varepsilon M_{BB}$$
 , 2.3

3. Stefan-Boltzmann Law

The total radiated energy from a unit area of a surface in a unit of time over a 2π steradian solid angle is called the radiant exitance of that surface. For blackbody source the radiance is proportional to the fourth power of the absolute temperature of the source. This gives [Ref. 4:p.45]

$$M(T) = \sigma T^4 \qquad , \qquad 2.4$$

where σ is the Stefan-Boltzmann constant =5.6697×10⁻¹² W-cm⁻²K⁻⁴

For use with non-black-body sources, this law is modified by the inclusion of an "effective emissivity", ϵ , giving the form

$$M(T)=\varepsilon\sigma T^4$$
, 2.5

where ε <1. For in-band radiance, the radiance N can be calculated using the universal blackbody curve or the proportional radiation table (Appendix B) with Equation 2.6

$$N = \frac{\varepsilon \sigma T^4}{\pi} \Delta q , \qquad 2.6$$

where

 ε = emissivity of the source.

 Δq = difference of two q values from the proportional radiation table (Appendix B)

The proportional radiation $q = f(\lambda, T)$ represents the fraction of the radiant exitance emitted by a blackbody at temperature T at all wavelengths up to the selected value of λ . It can be described in Equation 2.7

$$q = \frac{\int_0^{\lambda} M(\lambda, T) d\lambda}{\int_0^{\infty} M(\lambda, T) d\lambda} , \qquad 2.7$$

If q values are not shown on the table, they can be calculated by interpolation between two q value entries.

4. Kirchhoff's Law

When radiation is incident upon a body, some of it is transmitted, some absorbed, and some is reflected. Thus, the ratios of each of these to the incident power must add up to unity [Ref. 11:p. 1-29] given

$$\alpha(\lambda) + \rho(\lambda) + \tau(\lambda) = 1$$
, 2.8

where

 $\alpha(\lambda)$ = spectral absorptivity

 $\rho(\lambda)$ = spectral reflectivity

 $\tau(\lambda)$ = spectral transmissivity

5. Lambert-Beer Law

Atmospheric transmittance is a function of wavelength, which can be described by the Lambert-Beer law

$$\tau(\lambda)=e^{-\mu R}$$
,

where $\tau(\lambda)$ = spectral atmospheric transmittance,

 λ = wavelength,

 μ = extinction coefficient,

R = path length.

The extinction coefficient depends on the atmospheric molecular composition and aerosol concentration.

B. INFRARED RADIATION SOURCES

Optical sensors function by sensing the radiation emitted by an object or the radiation reflected from the object being illuminated by an external radiation source. Detection of a jet engine plume by an infrared detector is an example of the first category

whereas the visible detection of an area illuminated by the sun is an example of the second category. In both cases these sensors are passive, as they do not generate their own power. Active sensors on the other hand generate their own power and detect targets from the reflected energy of this power. Electro-optical systems may operate using natural and artificial sources of power.

C. ATMOSPHERIC PROPAGATION OF INFRARED RADIATION

The attenuation of optical radiation due to the atmosphere arises from the individual or collective effects of the following phenomena

- 1. Molecular absorption
- 2. Molecular scattering
- 3. Aerosol absorption
- 4. Aerosol scattering

The two main causes of attenuation, however, are molecular absorption by several minor constituents of the atmosphere and scattering due to atmospheric molecules and the particles in the present atmosphere (aerosols). Molecular absorption occurs mainly in several more or less narrow absorption bands and is due to transmittence in certain molecules, matched to that transition from one state of vibration and rotation to another, thereby absorbing or emitting a photon. [Ref. 4:p. 75]

1. Absorption Effects

Radiation absorption due to molecules in a gaseous medium can be divided into two processes:

(1) Atomic absorption is due to the transition of electrons in an atom, and usually requires a photon with an energy of a few electron volts. It generally takes place in the visible or ultraviolet region of the spectrum.

(2) Molecular absorption is due to a transition between electronic, vibrational, or rotational energy states of a gas molecule or due to a combination of all of these. This mechanism is dominant in the infrared range. [Ref. 4:p. 76]

2. Scattering Effects

Scattering is the process by which the energy in an electromagnetic wave is intercepted and reradiated into 4π steradians solid angle. It results from the interaction of the wave field with the electron oscillators in the scattering medium. These are excited by the incoming wave field, behaving as forced harmonic oscillators which reradiate at the frequency of the incident wave. The secondary wave, however, shows a phase lag from the primary dependent on the difference between the wave frequency and the oscillator resonance frequency. Any inhomogeneity in refractive index can cause scattering: in the atmosphere the component gas molecules, aerosol particles of various sizes, and fog, rain and hail drops are all effective scatters. The spatial distribution of the scattered radiation is strongly dependent on the relative magnitudes of the particle size and the wavelength. For particles very small compared with the wavelength, the scattering is approximately isotropic; as the ratio of size to wavelength increases, the scattering is concentrated more into the forward hemisphere. For very large scattering objects forward scattering dominates, and secondary lobes develop at other angles in the radiation pattern. In the small particle regime, the scattering can be described by the relatively simple theory developed by Rayleigh, which predicts scattering proportional to the second power of the volume of the wavelength. This describes scattering by atmospheric molecules. For particle sizes greater than one tenth of the wavelength, the Rayleigh approximation is no longer adequate; the more comprehensive Mie theory (1908) is required. [Ref. 7:p. 12-22]

a. Rayleigh Scattering

When the atmosphere does not contain large size particles, but only the

molecules of its gaseous constituents, the scattering phenomenon is dominated primarily by these molecules. The intensity of the scattering depends on the number and index of refraction of these gaseous molecules and on the scattering angle, wavelength, and polarization of the incident radiation. The attenuation of a light beam due to Rayleigh scattering is expressed by

$$I=I_0\exp(-\sigma_m R)$$
 , 2.10

where

 I_0 is the magnitude of the original radiation

I is the magnitude of the scattered radiation

 σ_m is the Rayleigh scattering coefficient

R is the path length

The Rayleigh scattering coefficient σ_m is the product of two parameters

$$\sigma_{\rm m} = \sigma_{\rm r} N$$
 , 2.11

where

 σ_r is the Rayleigh scattering cross section,

N is the molecular density.

The Rayleigh scattering cross section, σ_r , is defined as the cross section of an incident wave, so that the total power scattered by a gaseous molecule in all directions is equal to the power flowing across the cross section. It is given by the expression

$$\sigma_{\rm r} = \frac{8\pi^3 (n^2 - 1)^2}{3N^2 \lambda^4} , \qquad 2.12$$

where

n is the index of refraction of the gaseous medium

N is the molecular number density.

Note that the scattering cross section σ_r is a function of wavelength and proportional to λ^{-4} . It therefore dominates more in the ultraviolet and visible regions than in the infrared region. The formula also indicates that σ_r is a function of the index of refraction of air and molecular number density.[Ref. 4:p. 78]

b. Mie Scattering

Aerosol scattering, or Mie scattering, is concerned with the radiation interaction with spherical particles of various sizes. The transmitted beam irradiance here, similar to Rayleigh scattering, is expressed by

$$I=I_0\exp(-\sigma_a R)$$
, 2.13

where I, I_0 , and R are as defined previously, and σ_a is the aerosol attenuation coefficient, which is a function of aerosol density. Aerosol size distribution does not change much with altitude, whereas the aerosol density does. The relationship for aerosol attenuation coefficient at altitude h is given by

$$\sigma_a(h) = \frac{M(h)}{M(0)} \sigma_a(0) , \qquad 2.14$$

Where M(h) denotes the aerosol number density at height h and $\sigma_a(0)$ is the aerosol attenuation coefficient at sea level. [Ref. 4:p. 81] These absorption and scattering losses must be compounded when treating propagation through the atmosphere.

III. EOMET95 EXPERIMENT AND DATA COLLECTION

A. INTRODUCTION

The data for this thesis were obtained from an ocean field experiment conducted from 15 to 24 May 1995 off the coast of Monterey. The EOMET 95-Spring Cruise involved the R/V POINT SUR, which supported shipboard measurements of atmospheric and oceanic planetary boundary layer data made by the NPS Boundary Layer Meteorology group. In addition, measurements from stationary platforms located in Monterey Bay and its shoreline were collected. The R/V POINT SUR is a 135 foot ship (dimension: 41.5L×9.75W×8.8H (m)) owned by the National Science Foundation and operated by Moss Landing Marine Laboratory. Of particular interest was the availability of the POINT SUR during the mornings of the cruise for imaging operations, which placed the ship at various ranges, and aspect angles, which enabled the collection of polarized IR imager data coincident with the environmental measurements. During these operations, measurements were made of the degree of polarization and contrast improvement factor for ship images as a function of range and aspect angle. The environment impacts these measurements in the following ways:

- (1)The observed wave spectrum and wind speed/direction affects the sea surface degree of polarization.
- (2)The SST (Sea Surface Temperature) and air temperature impacts the target to background contrast.
- (3)The air temperature, humidity, and aerosol content affect the IR path radiance and extinction coefficient.

B. DATA MEASUREMENTS

1. Imaging System

The NPS AGA 780 Thermovision Thermal Imaging System was set up and operated from Moss Landing. The site was the MBARI Building located at approximately 6 meters above sea level. The estimated horizon range from this location was 4.5 nautical miles. The AGA 780 imaging system is a dual band serial scanning infrared imager capable of operation in the 3-5 and 8-14 micron bands. The system utilizes a 7×7 degree field of view lens or an optional 3.5 degree lens for each channel to focus incoming infrared radiation through a polarizing filter wheel, then through a dual rotating prism system onto the corresponding detector. The detectors are cooled to 77 K by dewars filled with liquid nitrogen. The filter wheel was rotated to provide vertical, horizontal and zero polarization settings during data collection. The detectors produce a current, which is called "thermal value" and is proportional to the intensity of the radiation received. The signal is then amplified and converted into a video signal for monitor display.

2. Calibration Technique

The AGA 780 imaging system was calibrated with a laboratory blackbody source. The system output or "thermal value " is recorded against the blackbody temperature through a range of temperatures. A calibration curve is generated which takes into account the scanner, lenses and filters (Moretz, 1994). All the data collected during EOMET 95 Spring Cruise was either calibrated or can be calibrated.

3. Target Temperature

To provide a means of determining target temperature, the R/V POINT SUR was instrumented with thermistor temperature sensors at numerous points on the ship's skin. Each thermistor was fastened to the skin by use of beryllium adhesive, which is extremely conductive. The thermistor was then covered with white epoxy to assure

maximum albedo from sunlight. The sensors were linked by shielded cable to a data collection computer in the instrumentation spaces aboard ship.

4. Visual Imaging

Coincident images in the visual range were made from the IR imager site at the MBARI building. These were made with a high quality video recorder system. The polarization analysis of these data will be presented in a further report or thesis.[Ref.8]

IV. MRTD AND MDTD

Minimum Detectable Temperature Difference (MDTD) and Minimum Resolvable Temperature Difference (MRTD) are two standard descriptions of FLIR performance. They are defined as those temperature contrast differences which make a standard bar chart just resolvable or a square target just detectable, respectively, to a trained observer. Each of these provides a sensitivity measurement of the FLIR system. Both of them employ the concept of the Equivalent Blackbody Temperature of a non-blackbody object. The equivalent blackbody temperature is that temperature a blackbody must have to emit the same radiance as the target. This allows the use of a single value to represent the target's temperature and emissivity. To complete the comparison of apparent ΔT with the system performance ΔT requires numerical values of these quantities as functions of spatial frequency and range.

A. MINIMUM RESOLVABLE TEMPERATURE DIFFERENCE

MRTD (often also abbreviated MRT) is a function of spatial frequency. It gives the ΔT between the hot (cold) and ambient temperature bars of a standard 4 bar (7:1 aspect ratio) chart required to make the bars just resolvable as a function of the spatial frequency of the bars. MRTD is a measure of the performance of the entire FLIR system. Since the MRTD includes the observer, the measurement is subjective. The computed system MRTD shows an asymptotic value beyond which the detector angular subtense is greater than the reciprocal of the spatial frequency, or the "spatial period" and finer detail cannot be distinguished. For a typical FLIR (Common Module), the instantaneous field of view (IFOV) is approximately 0.25 mRad so that the in-scan detector subtense Δx is approximately 0.25 mRad and the cut off spatial frequency (asymptote) is approximately $1/\Delta x=1/0.25=4$ cyc/mRad. If we use the "rule of thumb" asymptote between $0.7/\Delta x$ and

 $0.9/\Delta x$, we would find that the asymptote is approximately 3 cyc/mRad. The effective IFOV depends on the magnification of the optics that may be variable in some FLIRs.

Shumaker[Ref. 3:p. 8-52] gives a typical form for the MRTD.

$$MRT(v) = \frac{2 \text{ SNRT NET } \rho_{x}^{\frac{1}{2}}}{\text{MTF}_{S}(v)} \left[\frac{v^{2} \Delta x \Delta y}{L} \right]^{\frac{1}{2}} \left[t_{e} F_{r} N_{os} N_{ss} \right]^{-\frac{1}{2}}, \qquad 4.1$$

where SNRT = signal to noise ratio threshold,

NET = noise equivalent temperature,

 ρ_x = noise filter factor,

 $\Delta x = \text{in-scan detector subtense (mRad)},$

 $\Delta y = cross-scan detector subtense (mRad),$

MTF = modulation transfer function,

 ν = spatial frequency for which MRT is desired in cyc/mRad,

L = length-to- width ratio of the bar (7),

t_e = eye integration time in seconds,

Fr = frame rate s^{-1} ,

N_{os} = overscan ratio,

 N_{ss} = serial scan ratio.

Shumaker [Ref.3:p. 8-7] also provides an expression for the Noise Equivalent Temperature Difference (NET_D), the target apparent contrast ΔT which yields an output SNR of 1, as

$$NET_{D} = \frac{10(FOV_{x} FOV_{y} F_{r} N_{os} N_{ss})}{(\pi N_{D} \eta_{SC})^{1/2} D\Delta x \Delta y D * \eta_{CS} \partial N_{\sigma T} \tau_{0}}, \qquad 4.2$$

where $FOV_x = in\text{-scan } FOV \text{ in } mRad,$

FOV_y = cross-scan FOV in mRad,

 N_D = number of detectors,

 η_{sc} = scan efficiency,

 $\partial N/\partial T$ = derivative of Planck's equation in W/cm²-K-Sr,

 D^{**} = the band average detectivity in cm $Hz^{1/2}/W$,

D = aperture diameter in meters,

 $\tau_{\rm o}$ = transmission of the optics.

B. MINIMUM DETECTABLE TEMPERATURE DIFFERENCE

The MDTD of a FLIR system gives the temperature difference between an isolated square target and a uniform background that renders the square just detectable, as a function of the size of the square. In order to maintain similarity between graphs of MDTD and MRTD, MDTD is plotted as a function of the spatial frequency and range. Shumaker [Ref.3:p. 8-67] provides a typical form for MDTD

$$MDT(v) = \frac{\left(\text{SNRT}\right)\left(\text{NET}\right)\left(\Omega_T + r_S^2\right)\left(\Delta x \Delta y\right)^{\frac{1}{2}}}{\Omega_T \left[\frac{\pi}{4}\left(r_S^2 + r_B^2 + \Omega_T\right)t_e F_r N_{os} N_{ss}\right]^{\frac{1}{2}}},$$

$$4.3$$

where Ω_T = target angular subtense (mRad²),

 r_s = system resolution (mRad),

 r_B = back-end resolution (mRad).

The other definitions of the parameters in Equation 4.1 such as SNRT, NET, Δx , Δy , t_e , F_r , N_{os} , N_{ss} , are the same.

C. MRTD AND MDTD COMPUTATION

Shumaker[Ref.3:p.8-59] provides the following set of parameters that are postulated to be appropriate to the Common Module FLIR in NFOV (Narrow Field of View) mode. $\rho_X = (1 + (2v \cdot r_B)^2)^{-1/2}$ is computed from the equivalent back-end resolution r_B which is given for this example as 0.335 mRad.[Ref. 3:p. 8-60] The resulting

computation from MATLAB is shown in Figure 5 which shows MRTD and MDTD vs spatial frequency. MATLAB code is shown in Appendix J section B.

FOV _x	6.86°	FOV _Y	5.16°	L	7
F _r	30 sec ⁻¹	N _{os}	1	r _E	0.3 mRad
N _{ss}	1	N_{D}	180	r_d	0.08
$\eta_{ m sc}$	0.75	τ_0	0.70	N _s	2
t_e	0.1 sec	SNRT	2.5	MTF	Tabulated
f	0.20 m	Δy	0.25mRad	D,	4×10 ¹⁰
D	0.10 m	Δχ	0.25 mRad	NET	0.1°K

Table 1. Parameters of NFOV FLIR

Spatial Frequency (v)	$\Delta x = 0.25 \text{ mRad}$
(cyc/mRad)	MTF
0.00	1.00
0.25	0.89
0.50	0.79
0.75	0.64
1.00	0.53
1.25	0.43
1.50	0.35
1.75	0.27
2.00	0.20
2.50	0.10
3.00	0.04

Table 2. MTF for NFOV

V. DATA COMPUTATIONS AND ANALYSIS

A. APPARENT ΔT COMPUTATION

1. Data Summary of Infrared Measurements in EOMET95

The intent of the infrared imaging measurements made during the EOMET95 cruise was to observe the variation with range of the sea surface degree of polarization and of the apparent target/background temperature contrast improvement with polarization filtering for the R/V POINT SUR, and to attempt to observe emission polarization effects on facets of the ship image. To attain these ends the available ship operation periods were allotted alternately to two series of measurements;

- (1) Rotation of the POINT SUR by small increments of heading angle through 360° at fixed range and bearing from the sensor, for a selection of ranges and bearings. For each target aspect and range images were recorded with vertical and horizontal polarizing filter and no polarizer.
- (2) Recording of vertical and horizontally polarized and unpolarized images of the POINT SUR at selected aspect at a set of selected ranges along a constant bearing line to a maximum observation range.

Reference ship skin and sea and air temperature measurements were recorded during the entire observation period, as described below. Global Positional System (GPS) data for ship heading and position and radiosonde vertical atmospheric profiles were recorded on the R/V. POINT SUR. These values were accessed with the assistance of the NPS Boundary Layer Meteorology Group. The appropriate data selections are included in the appendices to this thesis.

For the purposes of this thesis certain data points were selected from this extensive data base, for calculation of predicted detection or recognition range.

2. Ship Temperature Computation

Ship skin temperature samples were collected from 15 thermistors attached with epoxy cement to the surfaces of the larger facets of the ship, located and distributed as indicated on Figure 12 and 13. The thermistor voltages were recorded continuously at 20 second intervals. The records were listed by time entries in seconds from midnight GMT for each day. These temperature files are listed in Appendix A. The format of the output files is illustrated by the sample file of Table 3. In each file the first header line gives the file name. The second line gives the Month, Day and Year from the computer clock, followed by the Hour, Minute and Second of the file on the next line. The next line gives the DAC voltage (digital value), start channel, stop channel, number of samples averaged, and reference channel number on each board. Note that thermistor channels 1 and 9 always read 25.00 °C since they are reference channels. The position data used in this analysis (extracted from the ship GPS data file listed in Appendix H for the period of IR measurement) are for the period from approximately 1830 to 1840 May 16 1995 GMT.

May 16.1

Mon, Day, Year 5 16 1995

Hour, Min, Sec= 8 27 36

volts, istart, istop, nsam, iref 1.49939 1 16 100 1

1326456 25.001 12.856 13.403 11.963 14.615 11.677 12.359 11.634 25.001 14.242 22.956 12.010 11.617 11.431 15.410 25.874

1326476 25.001 12.864 13.397 11.959 14.646 11.673 12.371 11.633 25.001 14.200 22.937 12.001 11.607 11.426 15.229 25.535

Table 3. File Identification for Ship Temperature Thermistor Reading

These thermistor readings provide ship temperature at selected points; from these an average ship temperature must be derived as input to a range estimation. This has been

done by comparing previous detailed radiometric measurements made of the temperature distribution over images of the R/V POINT SUR [Ref.9] with the concurrent thermistor spot temperature. From these data each facet area on the ship profile has been correlated with a representative thermistor location, as shown in Figure 13. Based on this correlation, an area weighting factor is assigned to each recorded thermistor temperature and a weighted average temperature computed for the appropriate ship aspect. While it is realized that the temperature distribution will change with change of ship operating conditions and meteorological conditions, this gives a relatively simple technique for modeling the ship signature, roughly comparable to methods previously used in Tactical Decision Aid models, and has been used here for the input ship temperature for the sample case. Table 7 shows ship average temperature for computation by equation 5.1.

Average temperature =
$$\frac{\sum T_i \Delta A_i}{\sum A_i}$$
, 5.1

3. Ship GPS Position and Heading Data Correlation

The times of recording of the ship GPS data and the skin temperature data are not synchronized. The temperature is recorded every 20 seconds while the position is recorded every 10 minutes. For accuracy in target signature modeling, recorded simultaneous ship heading and position values are selected from the GPS files (Appendix H), and the appropriate temperature values interpolated from the temperature files (Appendix A). As an example, to compute a detection/recognition range for the target at heading 120 degrees, the ship location and atmospheric parameters are interpolated between the measurement points in Appendix H closest to that heading, those entries highlighted in Appendix H. Data were recorded at 1830 GMT at heading 172 degrees, and 1840 GMT at 106 degrees. Interpolating to 120 degrees assuming a constant rotation rate of 66 degrees in 10 minutes, or 0.11 degrees per second, gives us a time of 18:37:53 GMT or 11:37:53 local time. To read the corresponding skin temperatures we convert this

time into seconds after the start of file at 08:27:36 at file number 1326456. This lapse time of 11416 seconds corresponds to file number 1337872. The closest skin temperature set to this is file number 1337876, shown in the sample listing below, highlighted in Appendix A, Page 65. It is assumed that no significant changes in meteorological parameters will occur in the 4 seconds discrepancy, so that the data selected for this time will form a consistent set.

1337856 25.001 16.392 17.862 17.334 15.415 15.885 14.338 15.873 25.001 18.294 24.326 15.281 16.169 15.352 22.299 28.721

<u>1337876 25.001 16.423 17.864 17.291 15.361 15.830 14.368 15.909 25.001 18.333</u> 24.164 15.296 16.151 15.346 22.393 28.829

1337896 25.001 16.458 17.844 17.241 15.295 15.771 14.383 15.946 25.001 18.366 24.093 15.304 16.117 15.305 22.319 28.933

Table 4. Thermistor Sample Output File

Side	Σ Pixel	Σ Temperature	ΣTemperature /ΣPixel
			= Average Temperature
Port	59	976.196	16.54569
Starboard	59	1028.287	17.42859
Total Average	118	2004.483	16.98714
Temperature			

Table 5. Ship Average Temperature vs Pixel for the Sample Case Selected

4. Temperature and Radiance Conversion

The average of ship temperature computed for this sample period is 273 + 16.987144 = 289.987144 K. Ship temperature and sea background temperature were

converted to in-band radiance by application of the Planck function. The ship temperature is then converted to in-band radiance $N_{\rm s}$ at zero range

$$N_s = \varepsilon \sigma T^4 \Delta q / \pi$$

= $0.95 \times 5.6697 \times 10^{-8} \times (289.98714)^4 \times 0.2486117/\pi = 30.14347844 \text{ (W/m}^2\text{Sr)}$ where

 ϵ =0.95, emissivity of R/V POINT SUR and Δq =q2-q1 is the fraction of the thermally emitted radiance lying in the band from λ_1 to λ_2 at source temperature T.

$$\lambda_1 T = 8\mu \times 289.98714 = 0.23198971 \text{ cm} \times K => q1 = 0.1314394$$

 $\lambda^2 T = 12\mu \times 289.98714 = 0.3479845 \text{ cm} \times K => q1 = 0.3800511$
and $\Delta q = q2 - q1 = 0.2486117$

The q values have 5 digits as reported in the radiation table (Appendix B) to keep the fraction of the radiant exitance as close as possible to the integral of Planck's Law.

5. Transmittance and Path Radiance

The SEARAD program was used to obtain the transmittance and path radiance between the target and the FLIR sensor. Appendix D describes how to install SEARAD and to run the example case. There are some points which need to be noted carefully when inserting radiosonde profile data in the input data file. The maximum number of atmospheric levels that can be inserted is 34. The position of every data point is important for SEARAD, so it is essential that each must be inserted in the correct column and row of the input table. The Windows text editor may cause a problem after the data have been inserted and saved. It is recommended that we use the simplest editor available (i.e. the MS-DOS editor). To run SEARAD it is not necessary to follow all the steps listed in Appendix D. "Tape 5" is the data file which will be read into SEARAD and executed; thus we need only modify the "Tape 5" data. The necessary steps to run SEARAD are shown below:

- Go to DOS program; it should show C:WINDOWS>.
- Under C:WINDOWS type "cd c:\".

- When it shows C:> then type "cd searad".
- It shows C:\searad> then type "edit tape5".
- It shows MS-DOS editor.
- Modify the data and save it; then exit.
- It should return to C:\searad>.
- Under C:\searad> type "searad" which means to execute SEARAD.
- We can use WORD or WORDPERFECT to read the output file "out" under the SEARAD directory.

The inputs of the SEARAD code are tabulated in Appendix F. The transmittance for this typical case is $\tau = 0.735$ and path radiance $N_p = 7.58028$ W/m²Sr. Ship radiance N_{s+p} at full range $=N_s \tau + N_p$

$$N_{s+p} = N_s \tau + N_p = 30.14347844 \times 0.735 + 7.58028 = 29.7357366 \text{ (W/m}^2\text{Sr)}$$

It is necessary to convert target radiance at maximum range to equivalent blackbody temperature. In-band radiance at full range can be converted into equivalent blackbody temperature by use of Planck's radiation law using an interactive computer program and look-up table as shown in Appendix C. As an example, when $N_{s+p} = 29.7357366 \text{ W/m}^2\text{Sr}$, the effective $T_{s+p} = 284.68 \text{ °K}$. From the SEARAD output (Appendix G shows a typical case), the background radiance N_b at full range is 21.93238 W/m²Sr. By conversion with the computer program in Appendix C, the corresponding apparent temperature is found to be 268.7 K. The apparent temperature difference at full range is then T_{s+p} - T_b =15.98 °C. The whole data set for the typical case are shown in Table 8.

B. MRTD AND MDTD VS RANGE COMPUTATION

1. Range, Elevation and Azimuth Angle

From GPS data (Appendix H) we must compute range and elevation and azimuth angles. There is a 7 hours time difference between GMT and local time (PACIFIC Summer Time). For example the time of 0800 for Monterey will be 1500 for GMT.

Appendix H contains the GPS data, for the time period in which the experiment took place. Figure 3 and 4 show the orientation of the ship and relation between bearing angle and ship's aspect. Since we treat the ship bow and stern aspects as the same, we only consider heading from zero to 180 degree in this thesis.

dx = (ship longitude)-(sensor longitude) (nmi)

dy = (ship latitude)-(sensor latitude) (nmi)

 $\alpha = \arctan(dx/dy) (degree)$

range =
$$\sqrt{dx^2 + dy^2}$$
 (nmi)

 θ = arctan ((sensor altitude) / range) (elevation angle)

To compute bearing we need to consider two different kinds of situation; those in which the ship is to the north or south of the sensor position. Range is computed by conversion of GPS location difference into distance.

a. Condition 1

dy>0. This is illustrated by Figure 3.

If heading > 180 -
$$\alpha$$
 , then β (bearing) = heading –180 + α

If heading
$$< 180 - \alpha$$
, then $\beta = 180 - \alpha$ - heading

b. Condition 2

dy<0. See Figure 4.

If heading $< \alpha$, then $\beta = \alpha$ – heading, if heading $> \alpha$, then β = heading – α

If
$$\beta < 90$$
 then $\phi = 90 - \beta$, if $\beta > 90$ then $\phi = 180 - \beta$

1 degree latitude at 37 degree N latitude is 59.97 nmi

1 degree longitude at 37 degree N latitude is 47.995 nmi

1 nmi (nautical mile) = 1.852 km = 1852 m

The computations are described in Appendix J section A,"MATLAB" code. After computation with previously selected data (see Table 8) we have:

$$\alpha = 38.6737 \text{ (degree)}$$

$$\beta \text{ (bearing)} = 21.3263 \text{ (degree)}$$

$$\text{range} = 0.7681 \text{ (nmi)} = 1.4225 \text{ (km)}$$

$$\phi = 1.1985 \text{ (rad) (azimuth angle)}$$

$$\theta = 0.0042 \text{ (rad) (elevation angle)}$$

2. Projected Area of the Ship A_t

From previous calculation we compute projected area.

$$A_T = lw \sin \theta + hw \cos \theta \sin \phi + hl \cos \theta \cos \phi$$

$$= 41.5 \cdot 9.75 \cdot \sin(0.0042) + 8.8 \cdot 9.75 \cdot \cos(0.0042) \sin(1.1985) + 41.5 \cdot 8.8 \cdot \cos(0.0042) \cos(1.1985)$$

$$= 214.4513 \, m^2$$

where

1 = 41.5 m (ship length) w = 9.75 m (ship width) h = 8.8 m (ship height) $\phi = 1.1985$ o (azimuth angle) $\theta = 0.0042$ (elevation angle) Figure 1 shows the orientation of a ship target model for calculating the projected area.

3. Critical Dimension D_c

The comparison of the temperature contrast of a ship target with the standard "bar target" for which the performance parameter MRTD is derived requires the definition of an equivalent resolved spatial frequency required on the target image for target recognition (or detection). In applying the long standing Johnson criterion [Ref.3:p. 2-7] of resolved cycles on the target, we adopt Moser's [Ref. 3:p. 2-6] convention for the "critical dimension" of the ship = $\sqrt{A_T}$ = 14.64 m. Dividing the critical dimension \mathcal{D}_c by the number of equivalent bars N on the target gives the physical dimension χ to be resolved (ie. pixel length) to accomplish the task, i.e. $\chi = D_c/N$. From the Johnson Criterion (see Table 6), the number of bars N necessary for pure detection, N = 1. The number of bars N necessary to classify the ship is 4 cyc × 2 bars/cyc = 8 bars. The number of bars N necessary to identify the ship is 6.4cyc x 2 bar/cyc = 12.8 bars. The one dimensional resolved "footprint" required on the target is then:

- a. For detection the physical dimension $\chi = D_c/N = 19.3/1 = 14.64 \text{ m}$
- b. For classification the physical dimension $\chi = D_c/N = 19.3/8 = 1.83 \text{ m}$
- c. For identification the physical dimension $\chi = D_c/N = 19.3/12.8 = 1.144 \text{ m}$

Discrimination Level	Cycles Across Minimum	Number of Bars
	Dimension	
Detection	1.0	1.0
Classification	4.0	8.0
Identification	6.4	12.8

Table 6. Johnson Criterion [Ref. 5:p. 54]

4. Conversion of Spatial Frequency to Range

The fundamental spatial frequency $f_{\rm c}$ characterizing the ship can be written in lines per milliradian as

$$f_c = \frac{R}{2000 \,\chi} \left(\text{cyc / m Rad} \right) \,, \qquad 5.2$$

where R is the range in meters from sensor to target. The relation of the spatial frequency to range R and physical dimension χ is shown in Figure 2. The MRTD and MDTD curves as a function of spatial frequency in NFOV for a generic Common Module FLIR have been given in Chapter IV and are shown plotted in Figure 5. The spatial frequency vs range relationship of Equation 5.1 has been used with Equation 4.1 and 4.2 to compute MRTD and MDTD vs range, for the R/V POINT SUR as target, using the required "cycles per critical dimension" N_c , in the form $\chi = D_c/N_c$, where N_c expresses the Moser definition of "critical dimension". The detailed calculations are in Appendix J, "MATLAB code". Figure 6 shows MRTD and MDTD for detection as function of range, for the R/V POINT SUR as target. The target available contrast temperature difference against background ΔT_{app} is also shown on the same range scale. The intersection points of ΔT with the MRTD and MDTD curves yield the maximum ranges for detection according to the two criteria. Figure 7 shows the corresponding MRTD for classification of the R/V POINT SUR, according to the Johnson criterion of required resolution line pairs on the critical dimension. MDTD cannot be used for classification. Figure 8 shows the equivalent curve for MRTD for identification of the POINT SUR. The value of $\Delta T_{app}(R)$ in these three figures is the simple estimate of ΔT_0 multiplied by the transmittance (see Section VI. A).

VI. DATA ANALYSIS AND CONCLUSIONS

The computations of target temperature difference ΔT , MDTD and MRTD for the experiment are described in the previous chapter. Meteorological data (including radiosonde measurement) for SEARAD code inputs were taken from the meteorological data that were recorded during the experiment, and are shown in Appendix H and Appendix I. The estimated MRTD curve and MDTD curve were derived from Shumaker's example 8-13[Ref. 3:p. 8-59] for a generic FLIR system in NFOV. The NET was chosen as 0.125 K, between 0.1 K to 0.25 K, due to degradation of the FLIR sensor after being in service for several years. This sensor is a generic common module FLIR model, with the parameters of Table 2. The condition for detection at maximum range is that the apparent target/background temperature difference as modified by atmospheric path attenuation and path radiance will match the required MDTD or MRTD at the same range. We have already expressed the MRTD and MDTD parameters as functions of range. We are now required to calculate the apparent temperature difference between target and background as a function of range from the target. Two methods of differing complexity are available for this computation; the greatly simplified approach of assuming that the temperature difference ΔT attenuates through the atmosphere in the same way as the irradiance, and the more complicated but more rigorous approach of converting the ΔT into a radiance difference, computing the transmitted radiance difference due to attenuation and path radiance, and reconverting ΔL back to ΔT_{app} through inversion of Planck's Law. Sample computations of both types have been made. These are compared in the following paragraphs, using the sample atmospheric data set of Table 8.

A. APPARENT ΔT BY ATTENUATION OF SOURCE ΔT

SEARAD with the "typical case" (see Table 8) scenario is found to give a transmittance of 0.735. Transmittance, averaged over a bandwidth which does not contain absorption edges, typically is written as an exponential function of range following Beer's Law. From transmittance we calculate attenuation coefficient averaged over the assumed bandpass of 8 to 12 µm, of

$$\tau = e^{-\mu R}$$
 => $\ln \tau = -\mu R$ => $\mu = \frac{-\ln \tau}{R}$
 $0.735 = e^{-\mu R}$ => $\ln(0.735) = -\mu(1.444 \text{km})$ => $\mu = 0.2132 \text{ km}^{-1}$

For transmittance $\tau = 0.735$ over a range of 1.4444 km for horizontal range 1.4225 km, the attenuation coefficient $\mu = 0.2132$ km⁻¹. The apparent temperature difference as a function of range is then computed with the form $\Delta T \times \tau(R) = \Delta T \times e^{-\mu R}$ using MATLAB. For a given target, the functions MRTD, MDTD and ΔT_{app} can be plotted on the same scale as functions of range. The intersection of the ΔT_{app} plot with the appropriate MRTD or MDTD curve occurs at the maximum range for the detection, classification or identification, according to the defined criterion. Figure 6 shows The MRTD-derived detection range as 21 km and the MDTD-derived value as 19 km. The classification range (from MRTD) is seen in Figure 7 to be 8.8 km. Figure 8 shows identification range as 6.2 km.

B. RADIANCE COMPUTATION METHOD

The second method of computation of effective ΔT is to convert the target and background temperatures to radiances, and compute the attenuated ΔT and appropriate path radiance for selected range, and reconvert the result into ΔT_{app} . This method was applied for a set of ranges appropriate to the measurement scenario and data set. Tables 9.1 to 9.5 show a tabulation of the computed parameters for the sensor elevation of 6 meters, the AGEMA imager location at Moss Landing. The locations were selected from

those for which observed images were recorded in EOMET95, so that the results may later be applied to comparisons of polarization. All the computed components of ΔT , the difference between the apparent values of ship average temperature corrected for attenuation and background temperature, are shown in this table. The independent variable is the zenith angle, used to define the path geometry for this sensor location. The zero range ship radiance is also input. The SEARAD program computes the corresponding range, transmittance and path radiance, and apparent ship radiance, and the background radiance. The radiance contrast is then converted back into temperature difference. Table 9.5 shows an anomaly in range and a path that does not intersect the sea surface beyond 13.3 km; this range defines the effective horizon for the selected sensor elevation of 6 meters. It follows that we cannot compute predicted maximum range for detection or recognition for ranges greater than this. To allow range predictions to be extended to greater ranges a further set of data was computed, for sensor elevation raised to 250 meters. This allows us to see range limitation by atmospheric effects rather than by geometry. The results of these computations are shown as Tables 10.1 to 10.6. From these tables we can see that ΔT attenuates almost to zero at long range. ΔT is shown plotted against range in Figure 9 and Figure 10. Figure 9 represents the original situation with sensor at 6 meters elevation; Figure 10 represents the same target and atmospheric scenario, but with the sensor raised to an elevation of 250 m. This revised curve allows the intersection of the $\Delta T(R)$ curve with MRTD(R) to be observed, and the Maximum Detection Range extracted. This curve is shown as Figure 11. Figure 14 shows ΔT vs MRTD for classification and identification. The apparent MRD is 44 km.

C. SEARAD

The SEARAD code input file requires the meteorological data inputs wind speed (W_S) , wind direction (W_D) , visibility (VIS), air mass character (AM) and the sea temperature. A sample input file for SEARAD is shown in Appendix F. The contents of the three header lines in Appendix F are defined by the "cards" listed in Appendix E.

Since SEARAD reads in the data it must to be in the correct column and row. The sample input file shows "card 2C1" which is for radiosonde data to be inserted. The last digit of the layer altitude must to be in column 10 and the last digit of pressure must be in column 20. The last digit for the temperature of the layer boundary must be in column 30 and the last digit of the relative humidity must be in column 40. The designated specific units must be in columns 61, 62 and 63. From the sample input file we can see they should be lined up column by column and row by row. The sample output from SEARAD (atmospheric transmittance τ and path radiance Np) are shown in Appendix G. To read in a new model atmosphere from radiosonde data, the sensor's altitude can not be greater than the upper layer boundary. SEARAD will use the altitude of the highest layer boundary rather than the sensor elevation. To use a high altitude sensor, it is necessary to use a higher layer boundary for the calculation of atmospheric transmittance τ and path radiance Np.

D. DISCUSSION OF THE DATA AND CONCLUSIONS

Based on a sample scenario selected from the data base of the EOMET95 measurement series in Monterey Bay off Moss Landing, ship skin temperature samples measured with a set of transistors were used with historical thermal distributions of the R/V POINT SUR, as measured radiometrically, to estimate an average ship temperature for the selected measurement time. From this together with the sea background temperature computed by SEARAD, a "zero range" contrast temperature difference ΔT was computed as 289.987 - 286.600 = 3.3871. This ΔT has been applied in two ways to estimate the Maximum Detection Range for the R/V POINT SUR. The first and simpler method is to assume that the contrast temperature difference, ΔT , is attenuated by the atmosphere in the same fashion as the radiance, ie $\Delta T_{app} = \Delta T_o e^{-\mu R}$. The second , more justifiable, method is to convert the temperature difference into in-band background radiance and target radiance, compute the corrections for attenuation and path radiance

using SEARAD, and reconvert to an apparent ΔT as a function of range. For each method ΔT_{app} is then compared with the MRTD or MDTD of the assumed sensor, as appropriate, also expressed as a function of range. The point of intersection then gives the maximum detection or recognition range. A weakness of this method is that the ship radiance is based solely on the thermal emission from the ship while the background calculation takes into account the reflected radiance also. The following observations are drawn from the results.

We see in Table 9 (page 53) and Figure 9 that the apparent temperature difference at short range initially increases. At 0.345 km ΔT_{app} is 21.18, much higher than the zero range value of 3.387. After reaching a peak value, the apparent temperature difference then decreases in an approximately exponential fashion with range.

For sensor altitude of 6 meters, beyond elevation angle 0.044, corresponding to a range of 13.262 km the calculated refracted path no longer intersects the earth surface. The path radiance cannot then be calculated, and the MDR cannot be calculated. This geometry is not appropriate for estimation of maximum detection range. The recalculation with assumed higher elevation for the sensor, required a redescription of the atmospheric layer structure, and allows calculation of the path radiance and surface radiance. We see in Table 10, with a sensor altitude of 250 m, ΔT_{app} has a value of 0.007 degrees at range 33.415 km, with zenith angle 0.550 degrees. The variation of ΔT_{app} with range (Figure 10) shows small differences from Figure 9. This must be ascribed to the reassignment of layer structure in SEARAD. The initial increase of ΔT_{app} at short range persists, and the curve is basically similar to Figure 9, except that it is extended to much longer ranges, so that estimation of MDR is possible. A comparison of the ΔT_{app} (R) as computed by the two methods is shown as Table 7.

A direct comparison of these range predictions indicates that the simple Beer's Law variation of $\Delta T_{app}(R)$ leads to an underestimation of the maximum range, relative to the SEARAD method including computed transmittance and path radiance. The values shown in Table 7 are comparable to values obtained in other range models. However a

factor of approximately 2 is apparent between the sets of results for detection with smaller differences for classification or identification. This point requires further discussion. The selection of the MDTD or MRTD criterion for detection appears to be of much lesser importance than the other differences between the model approaches.

	Detection	Classification	Identification
	Range	Range	Range
I. Extinction	MRTD: 21 km	MRTD: 8.8 km	MRTD:6.2 km
only	MDTD: 19 km		
II. SEARAD	MRTD: 47 km	MRTD: 13 km	MRTD:8 km
Correction	MDTD: 44 km		

Table. 7 Comparison of Two Methods

Some insight into the discrepancy may be gained by comparison of the transmittances calculated with the Beer's Law approach and the SEARAD code. Figure 15 shows this direct comparison. It can be seen that the Beer's Law method considerably underestimates the transmittance compared with direct computation. This is probably due to the band averaging over the 8 to 12 band, for which the apparent extinction coefficient decreases initially approaching a constant value only at longer ranges. The coefficient used in this analysis was deduced from extinction at 1.4 km, a measurement point in the EOMET95 data set. The differences observed in Figure 15 will decrease the discrepancy in predicted range but only in a minor way, as can be seen from the plot of apparent temperature difference shown as Figure 16. The SEARAD method shows negative values at very short range rising to values of up to 20° C, giving an increased effective ΔT_{o} , before decreasing in an approximately exponential fashion. The greatest factor in the range difference is this high ΔT_{o} . The SEARAD and Beer's Law methods use the same input radiometric sea surface temperature and thermometric target temperature. The SEARAD code then computes the sea surface radiance taking into account the sea surface

roughness and emissivity, and the reflection of sky radiance. The corresponding radiance temperature is then computed and used in the initial temperature ΔT_o . This procedure leads to the initial negative temperature difference seen in Tables 9 and 10, and in Figure 16. No equivalent radiance temperature model is available for the ship target.

The increase in ΔT_{app} at short ranges is an unexpected feature. Examination of Tables 9 and 10 shows that the ship radiance corrected for path radiance and transmittance decreases slowly and monotonically with range. The background radiance, however, decreases from a large initial value to a minimum occurring at 92° zenith angle for the 6 meter sensor and 95° for the 250 meter sensor, and then rises slowly at longer range. This behavior is not completely understood. It is non-intuitive that the sea radiance and the target radiance should behave differently at long range. The initial behavior at short range may be related to the variation of the emissivity and sky radiance. This behavior deserves further study.

It may be concluded that the use of SEARAD for range prediction constitutes a considerable improvement over the Beer's Law method. However a valid target signature radiance model is needed to give confidence in the predicted range. The SHIPSIG and THERMAL CONTRAST MODEL have been used in some previous prediction models, but are very specific to target and conditions, and so not convenient for general application. Addition of a simple facet ship signature representation to the ship orientation model is recommended.

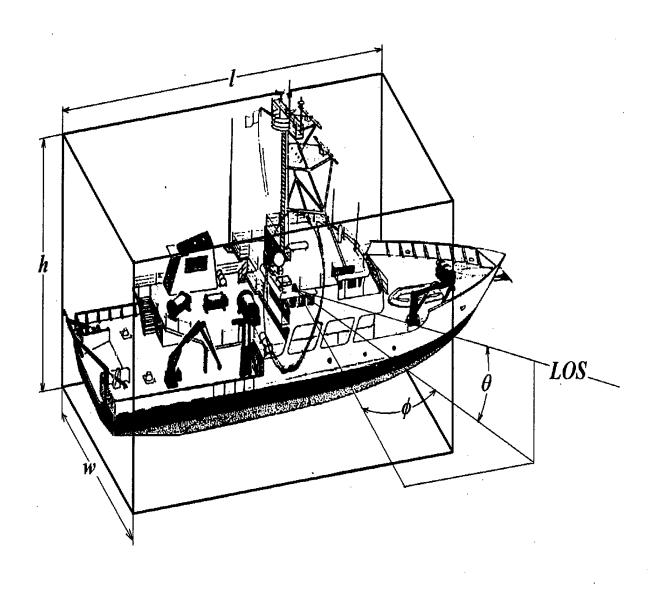
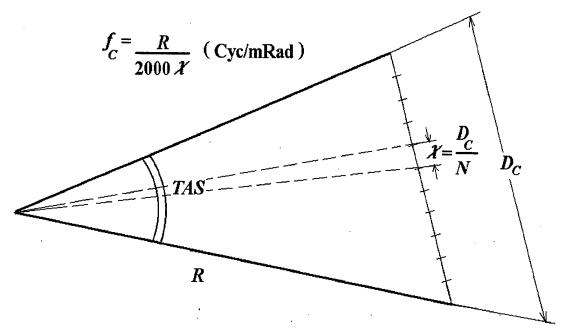


Figure 1. Orientation of Ship Target Model



N =Number of Bars in the Bar Chart

R = Slant Range

TAS = Target Angular Subtense

 D_C = Critical Dimension

 \mathcal{X} = Physical Dimension to be Resolved

 f_C = Spatial Frequency of Bar

Figure 2. Relation Between Spatial Frequency, Range R and Physical Dimension $\boldsymbol{\chi}$

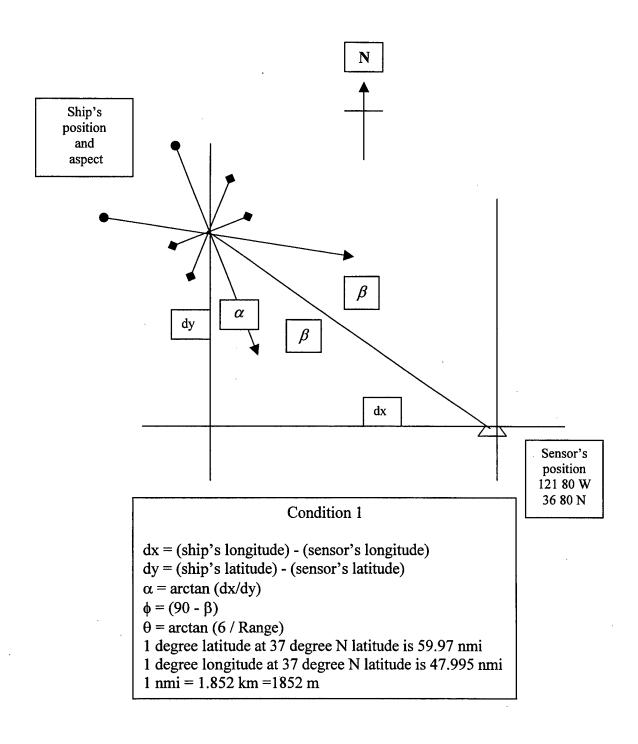


Figure 3. Relation Between GPS and Ship Aspect Condition 1

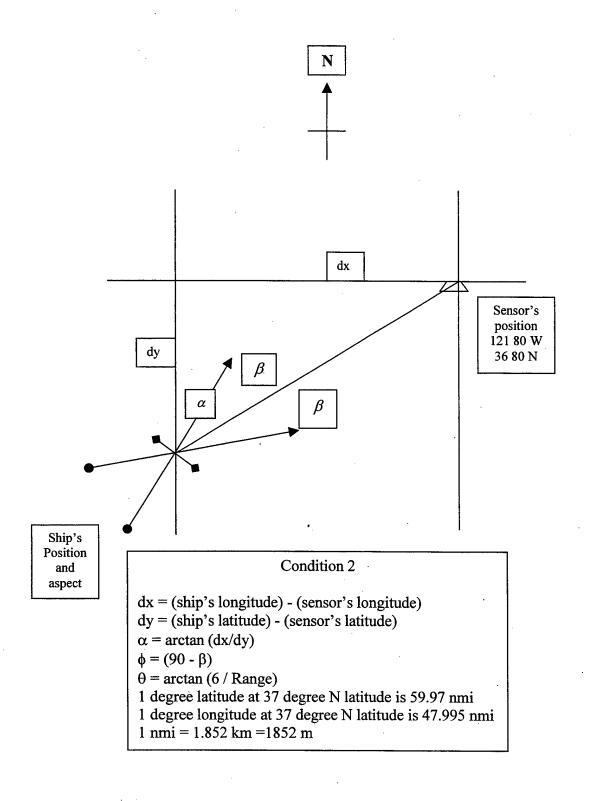


Figure 4. Relation Between GPS and Ship Aspect Condition 2

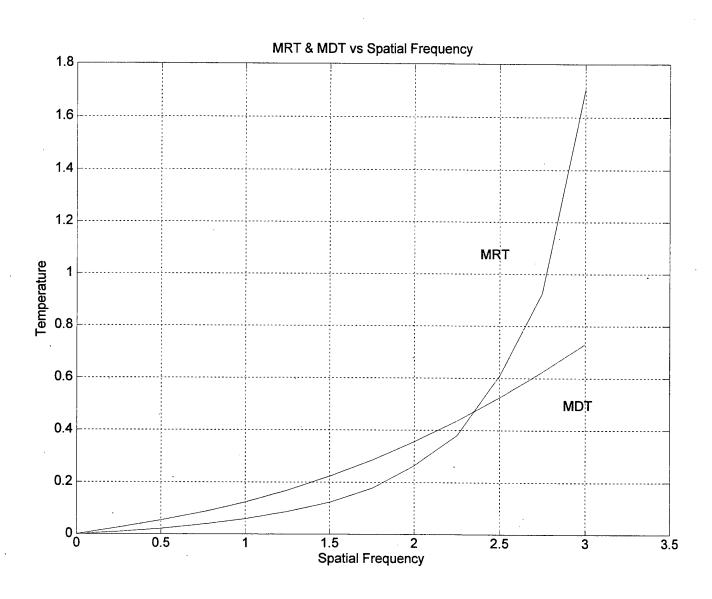


Figure 5. MRTD and MDTD as a Function of Spatial Frequency

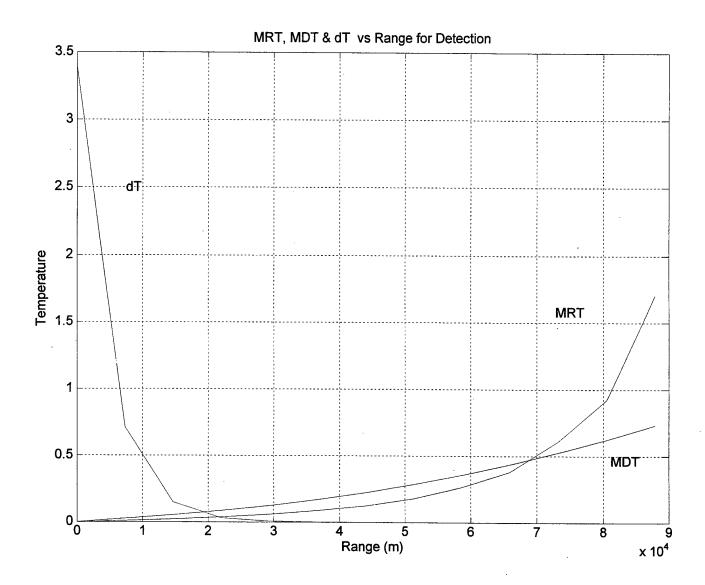


Figure 6. MRTD, MDTD and ΔT as a Function of Range for Detection

of R/V POINT SUR, ΔT by Beer's Law

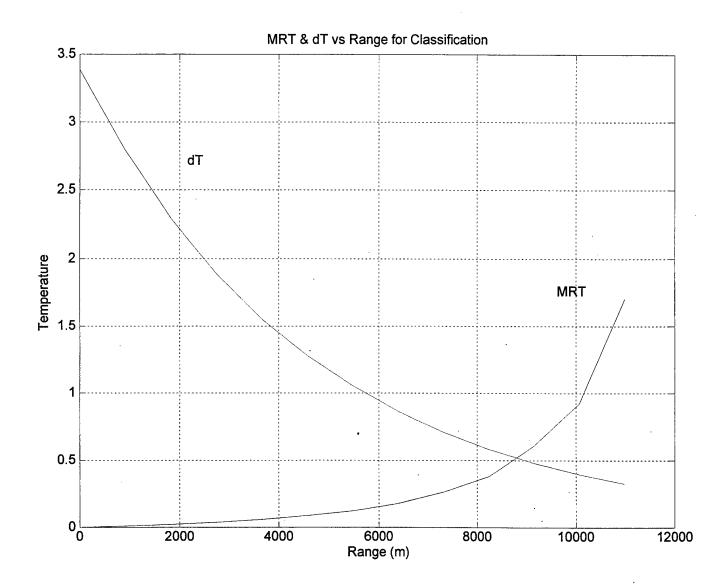


Figure 7. MRTD and ΔT as a Function of Range for Classification;

 ΔT by Attenuation of ΔT_0

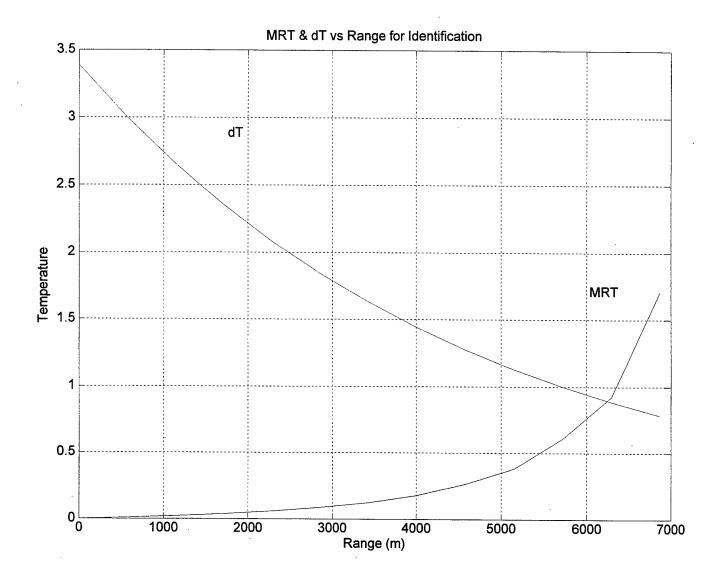


Figure 8. MRTD and ΔT as a Function of Range for Identification:

 ΔT by Attenuation of Source Method

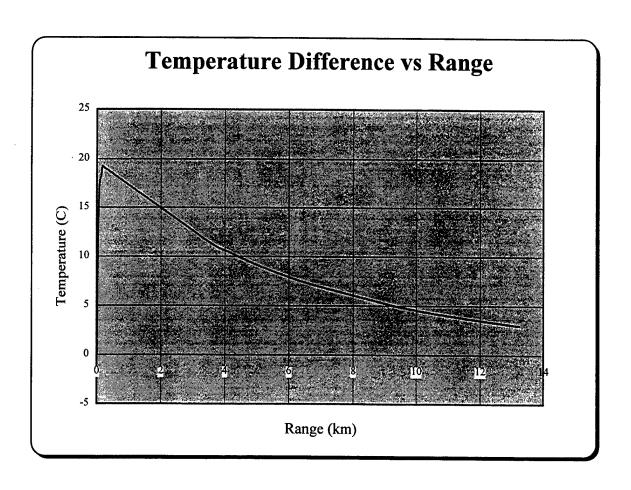


Figure 9. ΔT vs Range for Typical case, by Radiance Compensation Method, (SEARAD) Sensor at 6 meters Elevation

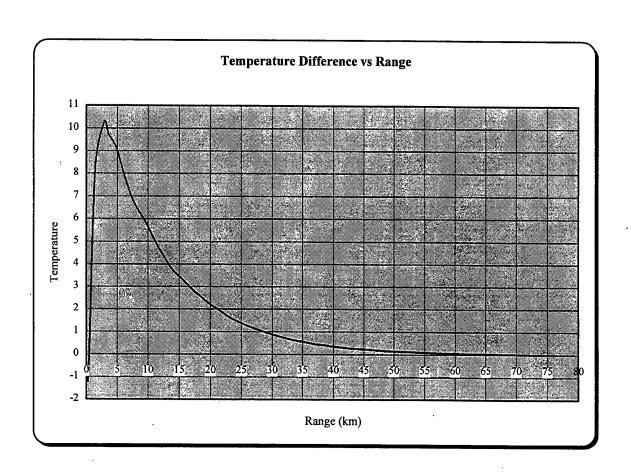


Figure 10. ΔT vs Range for MDR Estimate;

Sensor at 250 meters Elevation

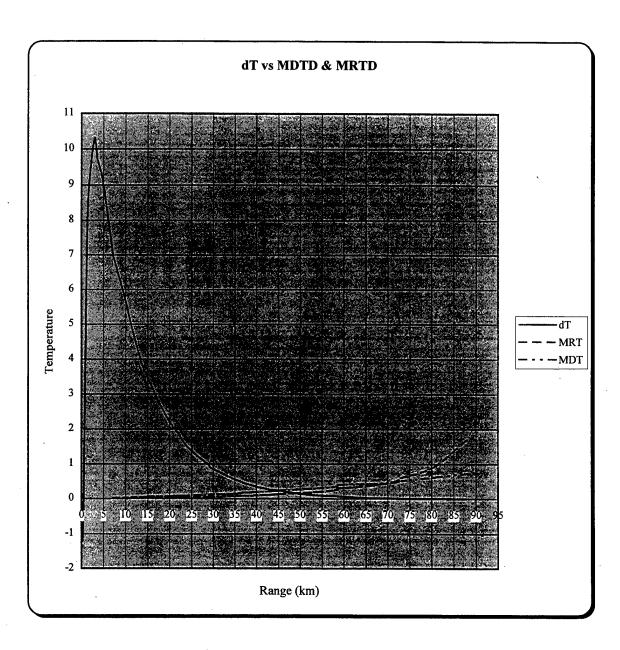


Figure 11. ΔT vs MRTD & MDTD for MDR Estimate

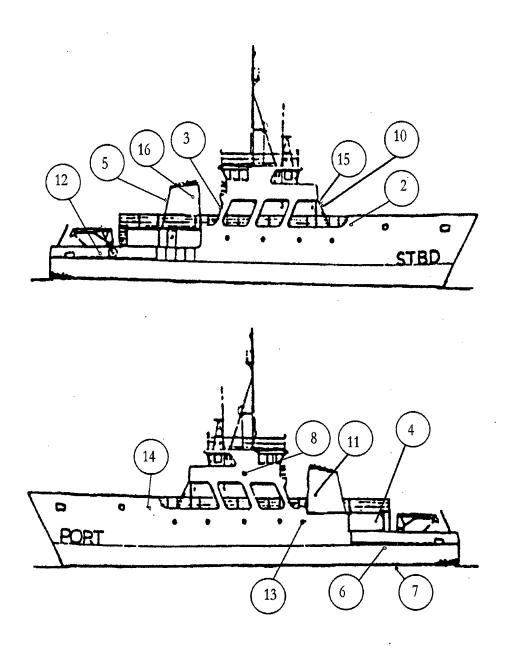
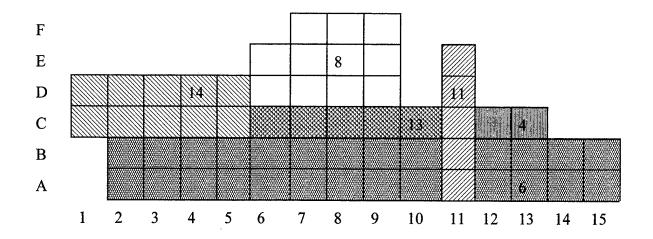


Figure 12. Locations of Thermistors

TEMPERATURE DISTRIBUTION TABLE, R/V POINT SUR PORT BEAM



TEMPERATURE DISTRIBUTION, R/V POINT SUR STARBOARD BEAM

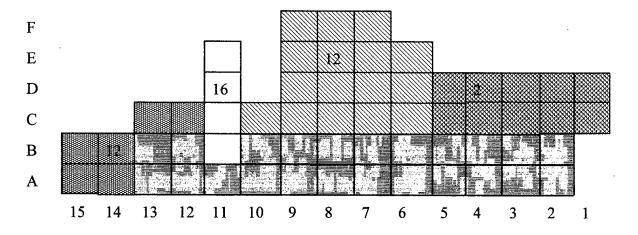


Figure 13. Distribution of Thermistors, and Correlation with Pixels

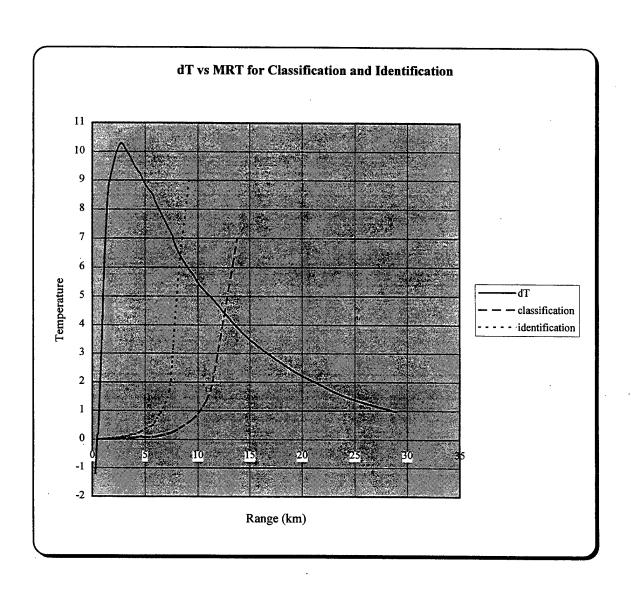


Figure 14. ΔT vs MRTD for Classification and Identification

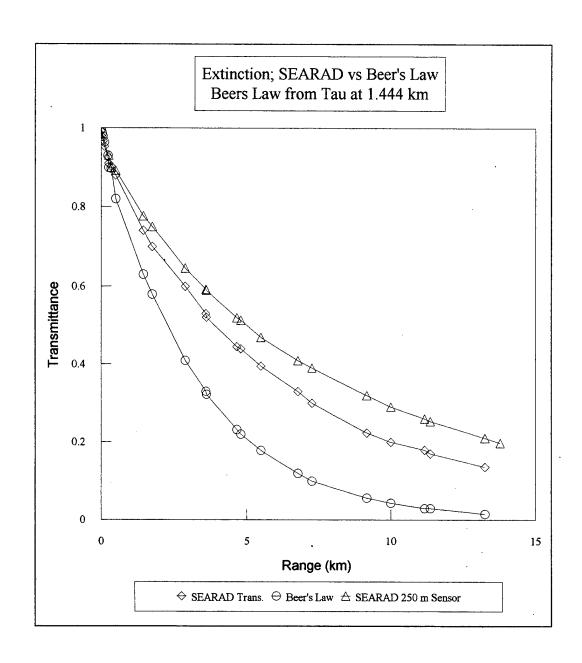


Figure 15. Comparison of Extinction; SEARAD vs Beer's Law

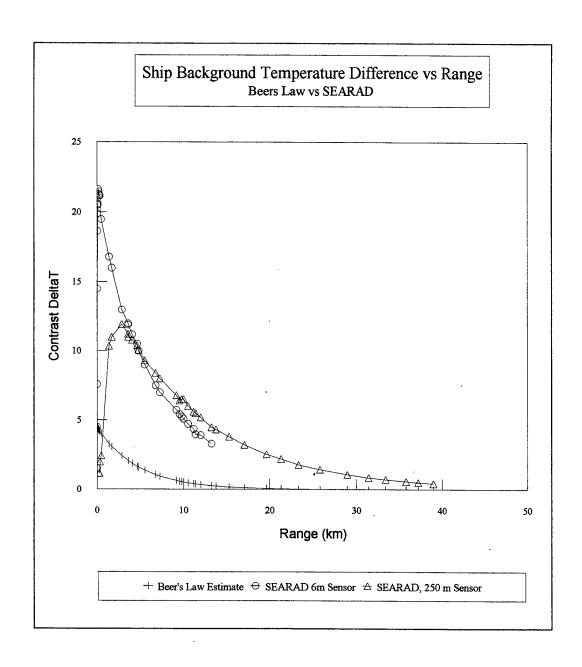


Figure 16. ΔT for Beer's Law vs SEARAD

Date 95/05/16 Time (GMT) 18:37:53 Time (local) 11:37:53 Ship Heading 120 Wind Speed (knot) 3.69 Wind Speed (m/s) 1.8966 Wind Speed (knot) 24-H Average 3.1201 Wind Speed (m/s) 24-H Average 1.6037 Wind Direction 252 Air Temperature (°C) 12.30 Relative Humility (%) 93.34 Pressure (mb) 1012 Latitude 36.81 N Longitude 121.81 W Ship Temperature (°C) 16.987144 Ship Temperature (°K) 289.987144 Sea Temperature (°C) 13.60 Sea Temperature (°K) 286.60 Ship Radiance Ns (zero range) 30.14347844 Transmittance τ 0.735 Path Radiance Np 7.58028 Ns×τ+Np=N _{s+p} 29.7357366 N _{s+p} ⇒ T _{s+p} 284.68 Background Radiance N _b 21.93238 N _b ⇒ T _b 268.7 T _{s+p} - T _b = ΔT _{app} 15.98	D-4-	05/05/46
Time (local) 11:37:53 Ship Heading 120 Wind Speed (knot) 3.69 Wind Speed (m/s) 1.8966 Wind Speed (knot) 24-H Average 3.1201 Wind Speed (m/s) 24-H Average 1.6037 Wind Direction 252 Air Temperature (°C) 12.30 Relative Humility (%) 93.34 Pressure (mb) 1012 Latitude 36.81 N Longitude 121.81 W Ship Temperature (°C) 16.987144 Ship Temperature (°K) 289.987144 Sea Temperature (°C) 13.60 Sea Temperature (°K) 286.60 Ship Radiance Ns (zero range) 30.14347844 Transmittance τ 0.735 Path Radiance Np 7.58028 Nsxt+Np=N _{s+p} 29.7357366 N _{s+p} \Rightarrow T _{s+p} 284.68 Background Radiance N _b 21.93238 N _b \Rightarrow T _b 268.7 T _{s+p} \rightarrow T _b \rightarrow T _b \rightarrow T _b 268.7 T _{s+p} \rightarrow T _b \rightarrow T _b \rightarrow T _b 15.98 Observe Range (km) 1.442 Azimuth angle (degree)		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		
Wind Speed (knot) 3.69 Wind Speed (m/s) 1.8966 Wind Speed (knot) 24-H Average 3.1201 Wind Speed (m/s) 24-H Average 1.6037 Wind Direction 252 Air Temperature (°C) 12.30 Relative Humility (%) 93.34 Pressure (mb) 1012 Latitude 36.81 N Longitude 121.81 W Ship Temperature (°C) 16.987144 Sea Temperature (°K) 289.987144 Sea Temperature (°C) 13.60 Sea Temperature (°K) 286.60 Ship Radiance Ns (zero range) 30.14347844 Transmittance τ 0.735 Path Radiance Np 7.58028 Ns× τ +Np=N _{s+p} 29.7357366 N _{s+p} \Rightarrow T _{s+p} 284.68 Background Radiance N _b 21.93238 N _b \Rightarrow T _b 268.7 T _{s+p} T _b \Rightarrow		
Wind Speed (knot) 24-H Average 3.1201 Wind Speed (m/s) 24-H Average 3.1201 Wind Speed (m/s) 24-H Average 1.6037 Wind Direction 252 Air Temperature (°C) 12.30 Relative Humility (%) 93.34 Pressure (mb) 1012 Latitude 36.81 N Longitude 121.81 W Ship Temperature (°C) 16.987144 Ship Temperature (°K) 289.987144 Sea Temperature (°C) 13.60 Sea Temperature (°C) 13.60 Sea Temperature (°K) 286.60 Ship Radiance Ns (zero range) 30.14347844 Transmittance τ 0.735 Path Radiance Np 7.58028 Ns× τ +Np=N _{s+p} 29.7357366 N _{s+p} \Rightarrow T _{s+p} 284.68 Background Radiance N _b 21.93238 N _b \Rightarrow T _b 268.7 T _{s+p} T _b \Rightarrow AT _{app} 15.98 Observe Range (km) 1.4425 Observe Range (km) 1.444 Bearing (degree) 21.326 Azimuth angle (degree) 6		
Wind Speed (knot) 24-H Average 3.1201 Wind Speed (m/s) 24-H Average 1.6037 Wind Direction 252 Air Temperature (°C) 12.30 Relative Humility (%) 93.34 Pressure (mb) 1012 Latitude 36.81 N Longitude 121.81 W Ship Temperature (°C) 16.987144 Ship Temperature (°K) 289.987144 Sea Temperature (°C) 13.60 Sea Temperature (°K) 286.60 Ship Radiance Ns (zero range) 30.14347844 Transmittance τ 0.735 Path Radiance Np 7.58028 Ns× τ +Np=N _{s+p} 29.7357366 N _{s+p} => T _{s+p} 284.68 Background Radiance N _b 21.93238 N _b => T _b 268.7 T _{s+p} - T _b = Δ T _{app} 15.98 Observe Range(km) horizontal 1.4225 Observe Range (km) 1.444 Bearing (degree) 21.326 Azimuth angle (degree) 68.674		3.69
Wind Speed (m/s) 24-H Average 1.6037 Wind Direction 252 Air Temperature (°C) 12.30 Relative Humility (%) 93.34 Pressure (mb) 1012 Latitude 36.81 N Longitude 121.81 W Ship Temperature (°C) 16.987144 Ship Temperature (°K) 289.987144 Sea Temperature (°C) 13.60 Sea Temperature (°K) 286.60 Ship Radiance Ns (zero range) 30.14347844 Transmittance τ 0.735 Path Radiance Np 7.58028 Ns× τ +Np=N _{s+p} 29.7357366 N _{s+p} => T _{s+p} 284.68 Background Radiance N _b 21.93238 N _b => T _b 268.7 T _{s+p} - T _b = Δ T _{app} 15.98 Observe Range(km) horizontal 1.4225 Observe Range (km) 1.444 Bearing (degree) 21.326 Azimuth angle (degree) 68.674	Wind Speed (m/s)	1.8966
Wind Direction 252 Air Temperature (°C) 12.30 Relative Humility (%) 93.34 Pressure (mb) 1012 Latitude 36.81 N Longitude 121.81 W Ship Temperature (°C) 16.987144 Ship Temperature (°K) 289.987144 Sea Temperature (°C) 13.60 Sea Temperature (°K) 286.60 Ship Radiance Ns (zero range) 30.14347844 Transmittance τ 0.735 Path Radiance Np 7.58028 Ns× τ +Np=N _{s+p} 29.7357366 Ns× τ +Np=N _{s+p} 29.7357366 Ns+p => T _{s+p} 284.68 Background Radiance N _b 21.93238 N _b => T _b 268.7 T _{s+p} - T _b = Δ T _{app} 15.98 Observe Range(km) horizontal 1.4225 Observe Range (km) 1.444 Bearing (degree) 21.326 Azimuth angle (degree) 68.674	Wind Speed (knot) 24-H Average	3.1201
Air Temperature (°C) 12.30 Relative Humility (%) 93.34 Pressure (mb) 1012 Latitude 36.81 N Longitude 121.81 W Ship Temperature (°C) 16.987144 Ship Temperature (°K) 289.987144 Sea Temperature (°C) 13.60 Sea Temperature (°K) 286.60 Ship Radiance Ns (zero range) 30.14347844 Transmittance τ 0.735 Path Radiance Np 7.58028 Ns× τ +Np=N _{s+p} 29.7357366 N _{s+p} >> T _{s+p} 284.68 Background Radiance N _b 21.93238 N _b => T _b 268.7 T _{s+p} - T _b = Δ T _{app} 15.98 Observe Range(km) horizontal 1.4225 Observe Range (km) 1.444 Bearing (degree) 21.326 Azimuth angle (degree) 68.674	Wind Speed (m/s) 24-H Average	1.6037
Relative Humility (%) 93.34 Pressure (mb) 1012 Latitude 36.81 N Longitude 121.81 W Ship Temperature (°C) 16.987144 Ship Temperature (°K) 289.987144 Sea Temperature (°C) 13.60 Sea Temperature (°K) 286.60 Ship Radiance Ns (zero range) 30.14347844 Transmittance τ 0.735 Path Radiance Np 7.58028 $Ns \times \tau + Np = N_{s+p}$ 29.7357366 $N_{s+p} \Rightarrow T_{s+p}$ 284.68 Background Radiance N_b 21.93238 $N_b \Rightarrow T_b$ 268.7 $T_{s+p} - T_b = \Delta T_{app}$ 15.98 Observe Range(km) horizontal 1.4225 Observe Range (km) 1.444 Bearing (degree) 21.326 Azimuth angle (degree) 68.674	Wind Direction	252
Pressure (mb) 1012 Latitude 36.81 N Longitude 121.81 W Ship Temperature (°C) 16.987144 Ship Temperature (°K) 289.987144 Sea Temperature (°C) 13.60 Sea Temperature (°K) 286.60 Ship Radiance Ns (zero range) 30.14347844 Transmittance τ 0.735 Path Radiance Np 7.58028 Ns×τ+Np=N _{s+p} 29.7357366 N _{s+p} ⇒ T _{s+p} 284.68 Background Radiance N _b 21.93238 N _b ⇒ T _b 268.7 T _{s+p} - T _b = ΔT _{app} 15.98 Observe Range(km) horizontal 1.4225 Observe Range (km) 1.444 Bearing (degree) 21.326 Azimuth angle (degree) 68.674	Air Temperature (°C)	12.30
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Relative Humility (%)	93.34
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Pressure (mb)	1012
Ship Temperature (°C) 16.987144 Ship Temperature (°K) 289.987144 Sea Temperature (°C) 13.60 Sea Temperature (°K) 286.60 Ship Radiance Ns (zero range) 30.14347844 Transmittance τ 0.735 Path Radiance Np 7.58028 Nsx τ +Np=N _{s+p} 29.7357366 N _{s+p} => T _{s+p} 284.68 Background Radiance N _b 21.93238 N _b => T _b 268.7 T _{s+p} - T _b = Δ T _{app} 15.98 Observe Range(km) horizontal 1.4225 Observe Range (km) 1.444 Δ T 3.387144 Bearing (degree) 21.326 Azimuth angle (degree) 68.674	Latitude	36.81 N
Ship Temperature (°K) 289.987144 Sea Temperature (°C) 13.60 Sea Temperature (°K) 286.60 Ship Radiance Ns (zero range) 30.14347844 Transmittance τ 0.735 Path Radiance Np 7.58028 Ns× τ +Np=N _{s+p} 29.7357366 N _{s+p} => T _{s+p} 284.68 Background Radiance N _b 21.93238 N _b => T _b 268.7 T _{s+p} - T _b = Δ T _{app} 15.98 Observe Range(km) horizontal 1.4225 Observe Range (km) 1.444 Δ T 3.387144 Bearing (degree) 21.326 Azimuth angle (degree) 68.674	Longitude	121.81 W
Sea Temperature (°C) 13.60 Sea Temperature (°K) 286.60 Ship Radiance Ns (zero range) 30.14347844 Transmittance τ 0.735 Path Radiance Np 7.58028 Ns× τ +Np=N _{s+p} 29.7357366 N _{s+p} => T _{s+p} 284.68 Background Radiance N _b 21.93238 N _b => T _b 268.7 T _{s+p} - T _b = Δ T _{app} 15.98 Observe Range(km) horizontal 1.4225 Observe Range (km) 1.444 Bearing (degree) 21.326 Azimuth angle (degree) 68.674	Ship Temperature (°C)	16.987144
Sea Temperature (°K) 286.60 Ship Radiance Ns (zero range) 30.14347844 Transmittance τ 0.735 Path Radiance Np 7.58028 Ns× τ +Np=N _{s+p} 29.7357366 N _{s+p} => T _{s+p} 284.68 Background Radiance N _b 21.93238 N _b => T _b 268.7 T _{s+p} - T _b = Δ T _{app} 15.98 Observe Range(km) horizontal 1.4225 Observe Range (km) 1.444 Δ T 3.387144 Bearing (degree) 21.326 Azimuth angle (degree) 68.674	Ship Temperature (°K)	289.987144
Ship Radiance Ns (zero range) 30.14347844 Transmittance τ 0.735 Path Radiance Np 7.58028 Ns× τ +Np=N _{s+p} 29.7357366 N _{s+p} => T _{s+p} 284.68 Background Radiance N _b 21.93238 N _b => T _b 268.7 T _{s+p} - T _b = Δ T _{app} 15.98 Observe Range(km) horizontal 1.4225 Observe Range (km) 1.444 Δ T 3.387144 Bearing (degree) 21.326 Azimuth angle (degree) 68.674	Sea Temperature (°C)	13.60
Transmittance τ 0.735 Path Radiance Np 7.58028 Ns×τ+Np=N _{s+p} 29.7357366 N _{s+p} => T _{s+p} 284.68 Background Radiance N _b 21.93238 N _b => T _b 268.7 T _{s+p} - T _b = Δ T _{app} 15.98 Observe Range(km) horizontal 1.4225 Observe Range (km) 1.444 Δ T 3.387144 Bearing (degree) 21.326 Azimuth angle (degree) 68.674	Sea Temperature (°K)	286.60
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	Ship Radiance Ns (zero range)	30.14347844
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	Transmittance τ	0.735
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	Path Radiance Np	7.58028
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Ns×τ+Np=N _{s+p}	29.7357366
$N_b \Rightarrow T_b$ 268.7 $T_{s+p} - T_b = \Delta T_{app}$ 15.98 Observe Range(km) horizontal 1.4225 Observe Range (km) 1.444 ΔT 3.387144 Bearing (degree) 21.326 Azimuth angle (degree) 68.674	$N_{s+p} => T_{s+p}$	284.68
$T_{s+p} - T_b = \Delta T_{app} $ 15.98 Observe Range(km) horizontal 1.4225 Observe Range (km) 1.444 $\Delta T $	Background Radiance N _b	21.93238
Observe Range(km) horizontal 1.4225 Observe Range (km) 1.444 ΔT 3.387144 Bearing (degree) 21.326 Azimuth angle (degree) 68.674	$N_b \Rightarrow T_b$	268.7
Observe Range (km) 1.444 ΔT 3.387144 Bearing (degree) 21.326 Azimuth angle (degree) 68.674	$T_{s+p} - T_b = \Delta T_{app}$	15.98
ΔT 3.387144 Bearing (degree) 21.326 Azimuth angle (degree) 68.674	Observe Range(km) horizontal	1.4225
Bearing (degree) 21.326 Azimuth angle (degree) 68.674	Observe Range (km)	1.444
Azimuth angle (degree) 68.674	. ΔΤ	3.387144
	Bearing (degree)	21.326
Elevation (degree) 0.24066	Azimuth angle (degree)	68.674
	Elevation (degree)	0.24066
Ship Project Area (m ²) 214.4513	Ship Project Area (m²)	214.4513

Table 8. Data File for Typical Case

Observed	Zero	0.006	0.021	0.039	0.000
Observed	Zelo	0.006	0.021	0.039	0.069
Range (km)	Range				
Zenith	0.0	158.500	107.000	99.000	95.000
Angle					
Emissivity	*****	0.9876	0.8518	0.6937	0.5887
3					
Ship Radiance	30.14347	30.14347	30.14347	30.14347	30.14347
Ns					
Transmittance	0.0	0.9924	0.9846	0.9773	0.9670
τ					;
Path Radiance	*****	0.19415	0.39946	0.59549	0.87565
Np					
Ns×τ+Np	*****	30.10853	30.07872	30.05470	30.02438
$=N_{S+P}$	·				
N _{S+P} convert to	*****	285.37	285.32	285.27	285.22
Temperature					
Background	*****	30.63620	27.41545	23.96328	22.04542
Radiance					
N _b convert to	*****	286.35	280.25	273.25	269.05
Temperature T _b					
$T_{S+P} - T_b = \Delta T$	3.387144	- 0.98	5.07	12.02	16.17
	L		<u> </u>		<u> </u>

Table 9.1 Data File for Typical Case Radiance Computation

	0.006	0.115	0.400	T	
Observed	0.086	0.115	0.138	0.172	0.230
Range (km)					
Zenith	94.000	93.000	92.500	92.000	91.500
Angle					
Emissivity	0.5613	0.5351	0.5227	0.5099	0.4954
ε					
Ship Radiance	30.14347	30.14347	30.14347	30.14347	30.14347
Ns					
Transmittance	0.9618	0.9538	0.9478	0.9393	0.9262
τ					
Path Radiance	1.01743	1.23811	1.40434	1.64105	2.01083
Np					
Ns×τ+Np	30.00941	29.9889	29.97432	29.95481	29.92926
$=N_{S+P}$		•			
N _{S+P} convert to	285.19	285.15	285.13	285.09	285.04
Temperature					
Background	21.46527	21.19206	21.14012	20.68977	20.70253
Radiance					
N _b convert to	267.75	267.05	266.95	265.85	265.95
Temperature T _b					
$T_{S+P} - T_b = \Delta T$	17.44	18.1	18.18	19.24	19.09
·					

Table 9.2 Data File for Typical Case Radiance Computation

99 90.200 20 0.4630	90.100	90.090	90.080
	90.100	90.090	90.080
	90.100	90.090	90.080
20 0.4630			
20 0.4630			
	0.4617	0.4616	0.4615
347 30.14347	7 30.14347	30.14347	30.14347
			·
23 0.6995	0.5210	0.4868	0.4457
34 8.63780	13.99925	15.03495	16.27719
379 29.72315	5 29.70399	29.70879	29.71213
96 284.66	284.62	284.63	284.64
745 22.26335	5 24.05040	24.40729	24.83836
09 269.40	273.4	274.1	275.03
7 15.57	11.22	10.53	9.61
ı			
	745 22.2633 09 269.40	745 22.26335 24.05040 09 269.40 273.4	745 22.26335 24.05040 24.40729 09 269.40 273.4 274.1

Table 9.3 Data File for Typical Case Radiance Computation

Observed	5.501	6.772	9.167	9.557	10.008
	5.501	0.772	9.107	9.557	10.008
Range (km)					
Zenith	90.070	90.060	90.050	90.049	90.048
Angle					
Emissivity	0.4614	0.4613	0.4611	0.4611	0.4611
€.					
Ship Radiance	30.14347	30.14347	30.14347	30.14347	30.14347
Ns			•		
Transmittance	0.3951	0.3298	0.2366	0.2243	0.2110
τ					
Path Radiance	17.80972	19.78584	22.60054	22.97070	23.37262
Np					
Ship Radiance	29.71940	29.72715	29.73248	29.73188	29.73289
N _{S+P}	, :				
N _{S+P} convert to	284.65	284.67	284.68	284.67	284.68
Temperature T _{S+P}					
Background Radiance	25.37396	26.06976	27.06865	27.20058	27.34404
N_{b}					
N _b convert to	276.15	277.57	279.56	279.83	280.11
Temperature T _b					
$T_{S+P} - T_b = \Delta T$	8.5	7.1	5.12	4.84	4.57

Table 9.4 Data File for Typical Case Radiance Computation

Observed	10.534	11.174	12.009	13.262	97.261
Range (km)					
Zenith	90.047	90.046	90.045	90.044	90.043
Angle					,
Emissivity	0.4611	0.4610	0.4610	0.4610	*****
ε	,				
Ship Radiance	30.14347	30.14347	30.14347	30.14347	30.14347
Ns					
Transmittance	0.1965	0.1802	0.1611	0.1363	0.0001
τ					
Path Radiance	23.80918	24.29645	24.86820	25.60797	*****
Np					
Ship Radiance	29.73237	29.72830	29.72431	29.71652	*****
N_{S+P}					
N _{S+P} convert to	284.66	284.67	284.66	284.65	*****
Temperature T _{S+P}					
Background Radiance	27.50002	27.67432	27.87898	28.14412	*****
N_b	·				
N _b convert to	280.43	280.75	281.15	281.67	*****
Temperature T _b					
$T_{S+P} - T_b = \Delta T$	4.23	3.92	3.51	2.98	*****

Table 9.5 Data File for Typical Case Radiance Computation

Observe	0.259	0.289	0.500	1.441	2.875
Range (km)					
Zenith	195.000	150.000	120.000	100.000	95.000
Angle	· ·	,			
Emissivity	0.9877	0.9869	0.9539	0.7180	0.5882
ε				·	
Ship Radiance	30.14347	30.14347	30.14347	30.14347	30.14347
· Ns					
Transmittance	0.9311	0.9258	0.8920	0.7764	0.6457
τ					
Path Radiance	1.86920	2.018832	2.97817	6.34750	10.23864
Np					
Ns×τ+Np	29.93578	29.92565	29.86614	29.75089	29.70227
$=N_{S+P}$					
N _{S+P} convert to	285.06	285.04	284.93	284.71	284.62
Temperature T _{S+P}					
Background Radiance	30.59705	30.57243	29.77694	25.48528	24.50860
N_{b}					
N _b convert to	286.27	286.23	284.76	276.35	274.35
Temperature T _b					
$T_{S+P} - T_b = \Delta T$	-1.21	-1.19	0.17	8.36	10.27
			·		

Table 10.1 Data File for MDR Computation

Observed Range	3.596	4.805	7.260	9.783	11.382
(km)).,05	11.502
Zenith	94.000	93.000	92.000	91.500	91.300
	71.000	75.000	72.000	71.500	91.500
Angle					
Emissivity	0.5607	0.5344	0.5084	0.4935	0.4882
ε '					
Ship Radiance	30.14347	30.14347	30.14347	30.14347	30.14347
Ns					
Transmittance	0.5919	0.5140	0.3909	0.2985	0.2526
τ	,				
Path Radiance	11.85932	14.21330	17.95142	20.76567	22.16049
Np					
Ns×τ+Np	29.70123	29.70704	29.73450	29.76349	29.77473
$=N_{S+P}$					
N _{S+P} convert to	284.62	284.63	284.68	284.73	284.76
Temperature T _{S+P}					·
Background Radiance	24.55046	25.01152	25.88875	26.76083	27.20808
N_b					
N _b convert to	274.9	275.49	277.7	278.95	279.85
Temperature T _b					
$T_{S+P} - T_b = \Delta T$	9.72	9.14	6.98	5.78	4.91
					·

Table 10.2 Data File for MDR Computation

Observed Range	13.776	15.334	17.098	19.663	21.299
(km)					
Zenith	91.090	90.990	90.900	90.800	90.750
Angle				:	
Emissivity	0.4818	0.4785	0.4756	0.4725	0.4709
ε					
Ship Radiance	30.14347	30.14347	30.14347	30.14347	30.14347
Ns					
Transmittance	0.1977	0.1690	0.1418	0.1101	0.0939
τ			,		
Path Radiance	23.82643	24.69582	25.51815	26.46917	26.95469
Np					:
Ns×τ+Np	29.78579	29.79006	29.79249	29.78796	29.78516
$=N_{S+P}$					
N _{S+P} convert to	284.77	284.78	284.79	284.78	284.78
Temperature T _{S+P}					
Background Radiance	27.73904	28.01768	28.28500	28.59857	28.76048
N_{b}					
N _b convert to	280.95	281.4	281.9	282.5	282.8
Temperature T _b					
$T_{S+P} - T_b = \Delta T$	3.82	3.38	2.89	2.28	1.98

Table 10.3 Data File for MDR Computation

Observed Range	23,278	25.743	28.948	31.421	33.415
(km)		2017.15	2015 10	31.121	33.113
Zenith	90.700	90.650	90.600	90.570	00.550
Zemin	90.700	90.630	90.000	90.570	90.550
Angle					
Emissivity	0.4694	0.4679	0.4664	0.4655	0.4649
ε					
Ship Radiance	30.14347	30.14347	30.14347	30.14347	30.14347
Ns	-				
Transmittance	0.0776	0.0613	0.0452	0.0358	0.0297
τ		:			
Path Radiance	27.44248	27.92743	28.40245	28.67854	28.85722
Np	·				
Ns×τ+Np	29.78161	29.77522	29.76493	29.75767	29.75248
$=N_{S+P}$		*			
N _{S+P} convert to	284.77	284.76	284.74	284.72	284.71
Temperature T _{S+P}					
Background Radiance	28.92441	29.08870	29.25099	29.34601	29.40779
$N_{\rm b}$					
N _b convert to	283.16	283.47	283.77	283.95	284.07
Temperature T _b					
$T_{S+P} - T_b = \Delta T$	1.61	1.29	0.97	0.77	0.64

Table 10.4 Data File for MDR Computation

Observed Range	35.809	37.210	38.962	39.310	42.769
(km)					
Zenith	90.530	90.520	90.509	90.507	90.490
Anala		7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	, , , , , ,	30.00) (1) (1)
Angle	0.4640	. 0.4640	0.4607	0.4505	0.4600
Emissivity '	0.4643	0.4640	0.4637	0.4636	0.4630
3					
Ship Radiance	30.14347	30.14347	30.14347	30.14347	30.14347
Ns					
Transmittance	0.0237	0.0208	0.0177	0.0171	0.0124
τ					
Path Radiance	29.03059	29.11495	29.20565	29.22193	29.35741
Np					
Ns×τ+Np	29.74499	29.74193	29.73918	29.73738	29.73118
$=N_{S+P}$:			
N _{S+P} convert to	284.70	284.69	284.69	284.68	284.67
Temperature T _{S+P}					
Background Radiance	29.46800	29.49740	29.52908	29.53478	29.58232
N_b			•		
N _b convert to	284.18	284.24	284.30	284.31	284.40
Temperature T _b					
$T_{S+P} - T_b = \Delta T$	0.52	0.45	0.39	0.37	0.27

Table 10.5 Data File for MDR Computation

Observed Range	45.409	48.877	54.146	58.641	71.559
(km)					
Zenith	90.480	90.470	90.460	90.455	90.450
Angle					
Emissivity	0.4626	0.4623	0.4618	0.4615	0.4610
ε					
Ship Radiance	30.14347	30.14347	30.14347	30.14347	30.14347
Ns					
Transmittance	0.0097	0.0070	0.0043	0.0028	0.0008
τ					
Path Radiance	29.43472	29.51111	29.58875	29.63071	29.68708
Np					
Ns×τ+Np	29.72711	29.72211	29.71836	29.71511	29.71111
$=N_{S+P}$			·		
N _{S+P} convert to	284.67	284.66	284.65	284.64	284.63
Temperature T _{S+P}					
Background Radiance	29.60958	29.63663	29.66433	29.67943	29.69996
N_b					
N _b convert to	284.44	284.50	284.55	284.58	284.62
Temperature T _b					
$T_{S+P} - T_b = \Delta T$	0.23	0.16	0.10	0.06	0.01

Table 10.6 Data File for MDR Computation

Channel	Location	Temperature	Pixel	Temp×Pixel
1	Reference	25.001	****	****
2	Starboard bow	16.423	10	164.23
3	Aft pilot house	17.864	****	****
4	Port aft of stack	17.291	2	34.582
5	Aft on stack	15.361	****	****
6	Aft port	15.830	26	411.58
7	Aft port water	14.368	****	****
8	Port pilot house	15.909	11	174.999
9	Reference	25.001	****	****
10	Bow pilot house	18.333	****	****
11	Port stack	24.164	5	120.82
12	Aft starboard	15.296	22	336.512
13	Port below stack	16.151	5	80.755
14	Port bow	15.346	10	153.46
15	Bow air	22.393	****	****
16	Starboard stack	28.829	4	115.316
**	Starboard above	17.923	23	412.229
	water-line			
Total	******	****	118	2004.483

Table 11. Distribution and Location of Thermistors

APPENDIX A. THERMISTOR SAMPLE OUTPUT FILE

May 16.1

Mon, Day, Year = 5 161995

Hour, Min, Sec = 8 27 36

volts,istart,istop,nsam,iref 1.49939 1 16 100 1

1326456 25.001 12.856 13.403 11.963 14.615 11.677 12.359 11.634 25.001 14.242 22.956 12.010 11.617 11.431 15.410 25.874

1326476 25.001 12.864 13.397 11.959 14.646 11.673 12.371 11.633 25.001 14.200 22.937 12.001 11.607 11.426 15.229 25.535

1326496 25.001 12.858 13.394 11.954 14.699 11.662 12.415 11.647 25.001 14.162 22.924 11.993 11.598 11.420 15.138 25.186

1326516 25.001 12.861 13.404 11.950 14.752 11.662 12.437 11.625 25.001 14.145 22.923 11.989 11.593 11.416 15.062 24.958

1337856 25.001 16.392 17.862 17.334 15.415 15.885 14.338 15.873 25.001 18.294 24.326 15.281 16.169 15.352 22.299 28.721

<u>1337876 25.001 16.423 17.864 17.291 15.361 15.830 14.368 15.909 25.001 18.333</u> 24.164 15.296 16.151 15.346 22.393 28.829

1337896 25.001 16.458 17.844 17.241 15.295 15.771 14.383 15.946 25.001 18.366 24.093 15.304 16.117 15.305 22.319 28.933

1337916 25.001 16.495 17.819 17.200 15.242 15.716 14.404 15.972 25.001 18.395 24.064 15.318 16.083 15.264 22.276 29.048

1337936 25.001 16.528 17.796 17.160 15.188 15.677 14.354 15.997 25.001 18.421 24.021 15.341 16.061 15.248 22.188 29.162

1337956 25.001 16.559 17.799 17.118 15.150 15.638 14.274 15.983 25.001 18.451 23.944 15.370 16.044 15.256 22.322 29.302

APPENDIX B. PROPORTIONAL RADIATION TABLE

The "Proportional Radiation", $q=f(\lambda$, T) represents the fraction of the radiant exitance which is emitted by a blackbody at temperature T at all wavelengths up to the selected values of λ . It is obtained from the integral over the Planck Law for wavelengths up to the selected values divided by the integral over all wavelengths, i.e.

$$q = \frac{\int\limits_{0}^{\lambda} M(\lambda T) d\lambda}{\int\limits_{0}^{\infty} M(\lambda T) d\lambda}$$

λT/cm K	q	λT/cm K	q	λT/cm K	q
			i I		
0.050	1.3652E-9	0.140	7.9035E-3	0.460	5.8075E-1
0.052	3.6788E-9	0.150	1.3023E-2	0.480	6.0880E-1
0.054	9.1749E-9	0.160	1.9962E-2	0.500	6.3494E-1
0.056	2.1358E-8	0.170	2.8858E-2	0.520	6.5912E-1
0.058	4.6745E-8	0.180	3.9754E-2	0.540	6.8146E-1
0.060	9.6798E-8	0.190	5.2613E-2	0.560	7.0209E-1
0.062	1.9069E-7	0.200	6.7331E-2	0.580	7.2116E-1
0.064	3.5907E-7	0.210	8.3750E-2	0.600	7.3877E-1
0.066	6.4902E-7	0.220	1.0168E-1	0.620	7.5507E-1
0.068	1.1302E-6	0.230	1.2091E-1	0.660	7.8402E-1
0.070	1.9025E-6	0.240	1.4122E-1	0.700	8.0885E-1
0.072	3.1045E-6	0.250	1.6239E-1	0.740	8.3020E-1
0.074	4.9236E-6	0.260	1.8423E-1	0.780	8.4861E-1
0.076	7.6070E-6	0.270	2.0653E-1	0.820	8.6455E-1
0.078	1.1473E-5	0.280	2.2911E-1	0.860	8.7840E-1
0.080	1.6923E-5	0.290	2.5183E-1	0.900	8.9048E-1
0.082	2.4453E-5	0.300	2.7454E-1	0.940	9.0100E-1
0.084	3.4668E-5	0.310	2.9712E-1	0.980	9.1033E-1
0.086	4.8287E-5	0.320	3.1947E-1	1.00	9.1455E-1
0.088	6.6159E-5	0.330	3.4150E-1	1.10	9.3217E-1
0.090	8.9269E-5	0.340	3.6314E-1	1.20	9.4532E-1

0.092	1.1874E-4	0.350	3.8432E-1	1.30	9.5331E-1
0.094	1.5586E-4	0.360	4.0502E-1	1.40	9.6304E-1
0.096	2.0204E-4	0.370	4.2518E-1	1.50	9.6909E-1
0.098	2.5885E-4	0.380	4.4479E-1	1.60	9.7390E-1
0.100	3.2804E-4	0.390	4.6382E-1	1.70	9.7777E-1
0.110	9.2957E-4	0.400	4.8227E-1	1.80	9.8091E-1
0.120	2.1727E-3	0.420	5.1738E-1	1.90	9.8349E-1
0.130	4.3866E-3	0.440	5.5012E-1	2.00	9.8563E-1

Adapted from "Optoelectronics; Theory and Practice" A. Chappell. Ed., McGraw-Hill Book Company, 1978

APPENDIX C. LOOK-UP TABLE

 $\label{eq:energy} In\mbox{-band Radiance (8-12$\mu m)} \\ and Apparent Temperature Conversion Look-up Table$

```
% Numerical Integration for Planck's law
% Integration by midpoint rule
% Matlab program with look-up table outputs
clear:
Tmin=291.; % <--- Guess T to obtain the corresponding radiance
dT=0.01;
n=200;
disp('Temperature
                     Radiance');
disp(' -----');
h=6.626e-34; c=2.998e8; k=1.382e-23;
a=8e-6; b=12e-6; dx=0.001e-6;
 for T=Tmin:dT:Tmin+n*dT
  sf=0.0;
  for x=a:dx:b-dx
                     % midpoint of f(x)
   xm=x+dx/2;
   f1=(2*h*c^2)/(xm^5);
   f2=1/(\exp((h*c)/(xm*k*T))-1);
   fx=f1*f2;
   sf=sf+fx*dx;
  end;
  disp([T,sf]);
end;
end;
(Liu, 1996)
```

Look-up Table for Temperature and Radiance Conversions

Temp	Radiance	Temp	Radiance	Temp	Radiance	Temp	Radiance
283.0000	28.8410	283.0100	28.8463	283.0200	28.8515	283.0300	28.8568
283.0400	28.8621	283.0500	28.8673	283.0600	28.8726	283.0700	28.8779
283.0800	28.8832	283.0900	28.8884	283.1000	28.8937	283.1100	28.8990
283.1200	28.9042	283.1300	28.9095	283.1400	28.9148	283.1500	28.9201
283.1600	28.9253	283.1700	28.9306	283.1800	28.9359	283.1900	28.9412
283.2000	28.9464	283.2100	28.9517	283.2200	28.9570	283.2300	28.9623
283.2400	28.9676	283.2500	28.9728	283.2600	28.9781	283.2700	28.9834
283.2800	28.9887	283.2900	28.9940	283.3000	28.9993	283.3100	29.0045
283.3200	29.0098	283.3300	29.0151	283.3400	29.0204	283.3500	29.0257
283.3600	29.0310	283.3700	29.0363	283.3800	29.0415	283.3900	29.0468
283.4000	29.0521	283.4100	29.0574	283.4200	29.0627	283.4300	29.0680
283.4400	29.0733	283.4500	29.0786	283.4600	29.0839	283.4700	29.0892
283.4800	29.0945	283.4900	29.0998	283.5000	29.1051	283.5100	29.1104
283.5200	29.1157	283.5300	29.1210	283.5400	29.1263	283.5500	29.1316
283.5600	29.1369	283.5700	29.1422	283.5800	29.1475	283.5900	29.1528
283.6000	29.1581	283.6100	29.1634	283.6200	29.1687	283.6300	29.1740
283.6400	29.1793	283.6500	29.1846	283.6600	29.1899	283.6700	29.1952
283.6800	29.2005	283.6900	29.2058	283.7000	29.2111	283.7100	29.2164
283.7200	29.2217	283.7300	29.2270	283.7400	29.2323	283.7500	29.2377
283.7600	29.2430	283.7700	29.2483	283.7800	29.2536	283.7900	29.2589
283.8000	29.2642	283.8100	29.2695	283.8200	29.2749	283.8300	29.2802
283.8400	29.2855	283.8500	29.2908	283.8600	29.2961	283.8700	29.3014
283.8800	29.3068	283.8900	29.3121	283.9000	29.3174	283.9100	29.3227
283.9200	29.3280	283.9300	29.3334	283.9400	29.3387	283.9500	29.3440
283.9600	29.3493	283.9700	29.3547	283.9800	29.3600	283.9900	29.3653

284.0000	29.3706	284.0100	29.3760	284.0200	29.3813	284.0300	29.3866
284.0400	29.3920	284.0500	29.3973	284.0600	29.4026	284.0700	29.4079
284.0800	29.4133	284.0900	29.4186	284.1000	29.4239	284.1100	29.4293
284.1200	29.4346	284.1300	29.4399	284.1400	29.4453	284.1500	29.4506
284.1600	29.4559	284.1700	29.4613	284.1800	29.4666	284.1900	29.4720
284.2000	29.4773	284.2100	29.4826	284.2200	29.4880	284.2300	29.4933
284.2400	29.4987	284.2500	29.5040	284.2600	29.5093	284.2700	29.5147
284.2800	29.5200	284.2900	29.5254	284.3000	29.5307	284.3100	29.5361
284.3200	29.5414	284.3300	29.5468	284.3400	29.5521	284.3500	29.5574
284.3600	29.5628	284.3700	29.5681	284.3800	29.5735	284.3900	29.5788
284.4000	29.5842	284.4100	29.5895	284.4200	29.5949	284.4300	29.6003
284.4400	29.6056	284.4500	29.6110	284.4600	29.6163	284.4700	29.6217
284.4800	29.6270	284.4900	29.6324	284.5000	29.6377	284.5100	29.6431
284.5200	29.6485	284.5300	29.6538	284.5400	29.6592	284.5500	29.6645
284.5600	29.6699	284.5700	29.6753	284.5800	29.6806	284.5900	29.6860
284.6000	29.6913	284.6100	29.6967	284.6200	29.7021	284.6300	29.7074
284.6400	29.7128	284.6500	29.7182	284.6600	29.7235	284.6700	29.7289
284.6800	29.7343	284.6900	29.7396	284.7000	29.7450	284.7100	29.7504
284.7200	29.7557	284.7300	29.7611	284.7400	29.7665	284.7500	29.7719
284.7600	29.7772	284.7700	29.7826	284.7800	29.7880	284.7900	29.7934
284.8000	29.7987	284.8100	29.8041	284.8200	29.8095	284.8300	29.8149
284.8400	29.8202	284.8500	29.8256	284.8600	29.8310	284.8700	29.8364
284.8800	29.8418	284.8900	29.8471	284.9000	29.8525	284.9100	29.8579
284.9200	29.8633	284.9300	29.8687	284.9400	29.8740	284.9500	29.8794
284.9600	29.8848	284.9700	29.8902	284.9800	29.8956	284.9900	29.9010
285.0000	29.9064	285.0100	29.9118	285.0200	29.9171	285.0300	29.9225
285.0400	29.9279	285.0500	29.9333	285.0600	29.9387	285.0700	29.9441
285.0800	29.9495	285.0900	29.9549	285.1000	29.9603	285.1100	29.9657

285.1200	29.9711	285.1300	29.9765	285.1400	29.9819	285.1500	29.9872
285.1600	29.9926	285.1700	29.9980	285.1800	30.0034	285.1900	30.0088
285.2000	30.0142	285.2100	30.0196	285.2200	30.0250	285.2300	30.0304
285.2400	30.0358	285.2500	30.0412	285.2600	30.0467	285.2700	30.0521
285.2800	30.0575	285.2900	30.0629	285.3000	30.0683	285.3100	30.0737
285.3200	30.0791	285.3300	30.0845	285.3400	30.0899	285.3500	30.0953
285.3600	30.1007	285.3700	30.1061	285.3800	30.1115	285.3900	30.1169
285.4000	30.1224	285.4100	30.1278	285.4200	30.1332	285.4300	30.1386
285.4400	30.1440	285.4500	30.1494	285.4600	30.1548	285.4700	30.1603
285.4800	30.1657	285.4900	30.1711	285.5000	30.1765	285.5100	30.1819
285.5200	30.1874	285.5300	30.1928	285.5400	30.1982	285.5500	30.2036
285.5600	30.2090	285.5700	30.2145	285.5800	30.2199	285.5900	30.2253
285.6000	30.2307	285.6100	30.2362	285.6200	30.2416	285.6300	30.2470
285.6400	30.2524	285.6500	30.2579	285.6600	30.2633	285.6700	30.2687
285.6800	30.2741	285.6900	30.2796	285.7000	30.2850	285.7100	30.2904
285.7200	30.2959	285.7300	30.3013	285.7400	30.3067	285.7500	30.3122
285.7600	30.3176	285.7700	30.3230	285.7800	30.3285	285.7900	30.3339
285.8000	30.3393	285.8100	30.3448	285.8200	30.3502	285.8300	30.3557
285.8400	30.3611	285.8500	30.3665	285.8600	30.3720	285.8700	30.3774
285.8800	30.3829	285.8900	30.3883	285.9000	30.3937	285.9100	30.3992
285.9200	30.4046	285.9300	30.4101	285.9400	30.4155	285.9500	30.4210
285.9600	30.4264	285.9700	30.4319	285.9800	30.4373	285.9900	30.4427
286.0000	30.4482	286.0100	30.4536	286.0200	30.4591	286.0300	30.4645
286.0400	30.4700	286.0500	30.4754	286.0600	30.4809	286.0700	30.4864
286.0800	30.4918	286.0900	30.4973	286.1000	30.5027	286.1100	30.5082
286.1200	30.5136	286.1300	30.5191	286.1400	30.5245	286.1500	30.5300
286.1600	30.5355	286.1700	30.5409	286.1800	30.5464	286.1900	30.5518
286.2000	30.5573	286.2100	30.5628	286.2200	30.5682	286.2300	30.5737

0.6229 0.6448 0.6666 0.6885 0.7105 0.7324	286.4900	30.6283 30.6502 30.6721 30.6940	*****	30.6338 30.6557 30.6776	286.3100 286.3500 286.3900 286.4300	30.6174 30.6393 30.6612 30.6831
0.6448 0.6666 0.6885 0.7105 0.7324	286.3700 286.4100 286.4500 286.4900	30.6502 30.6721 30.6940	286.3800 286.4200 286.4600	30.6557 30.6776	286.3900 286.4300	30.6612 30.6831
2.6666 2.6885 2.7105 2.7324	286.4100 286.4500 286.4900	30.6721 30.6940	286.4200 286.4600	30.6776	286.4300	30.6831
.7105 .7324	286.4500 286.4900	30.6940	286.4600			
.7105	286.4900		*****	30.6995	286 4700	
.7324		30.7159			200.7700	30.7050
	207 5200		286.5000	30.7214	286.5100	30.7269
	286.5300	30.7379	286.5400	30.7433	286.5500	30.7488
.7543	286.5700	30.7598	286.5800	30.7653	286.5900	30.7708
.7762	286.6100	30.7817	286.6200	30.7872	286.6300	30.7927
.7982	286.6500	30.8037	286.6600	30.8092	286.6700	30.8147
.8201	286.6900	30.8256	286.7000	30.8311	286.7100	30.8366
.8421	286.7300	30.8476	286.7400	30.8531	286.7500	30.8586
.8641	286.7700	30.8696	286.7800	30.8751	286.7900	30.8806
.8861	286.8100	30.8916	286.8200	30.8971	286.8300	30.9026
.9081	286.8500	30.9136	286.8600	30.9191	286.8700	30.9246
.9301	286.8900	30.9356	286.9000	30.9411	286.9100	30.9466
.9521	286.9300	30.9576	286.9400	30.9631	286.9500	30.9686
.9741	286.9700	30.9796	286.9800	30.9851	286.9900	30.9906
.9962	287.0000	30.9962	287.0100	31.0017	287.0200	31.0072
.0127	287.0400	31.0182	287.0500	31.0237	287.0600	31.0292
.0347	287.0800	31.0403	287.0900	31.0458	287.1000	31.0513
.0568	287.1200	31.0623	287.1300	31.0678	287.1400	31.0734
.0789	287.1600	31.0844	287.1700	31.0899	287.1800	31.0954
.1010	287.2000	31.1065	287.2100	31.1120	287.2200	31.1175
.1231	287.2400	31.1286	287.2500	31.1341	287.2600	31.1396
.1452	287.2800	31.1507	287.2900	31.1562	287.3000	31.1617
.1673	287.3200	31.1728	287.3300	31.1783	287.3400	31.1839
	.7543 .7762 .7982 .8201 .8421 .8641 .9301 .9521 .9741 .9962 .0127 .0347 .0568 .0789 .1010 .1231	.0568 287.1200 .0789 287.1600 .1010 287.2000 .1231 287.2400 .1452 287.2800	.7324286.530030.7379.7543286.570030.7598.7762286.610030.7817.7982286.650030.8037.8201286.690030.8256.8421286.730030.8476.8641286.770030.8696.8861286.810030.9136.9081286.850030.9136.9521286.930030.9576.9741286.970030.9796.9962287.000030.9962.0127287.040031.0182.0347287.080031.0403.0568287.120031.0623.0789287.160031.0844.1010287.200031.1286.1231287.240031.1286.1452287.280031.1507	.7543286.570030.7598286.5800.7762286.610030.7817286.6200.7982286.650030.8037286.6600.8201286.690030.8256286.7000.8421286.730030.8476286.7400.8641286.770030.8696286.7800.8861286.810030.8916286.8200.9081286.850030.9136286.8600.9301286.890030.9356286.9000.9521286.930030.9576286.9400.9741286.970030.9796286.9800.9962287.000030.9962287.0100.0127287.040031.0182287.0500.0347287.080031.0403287.0900.0568287.120031.0623287.1300.0789287.160031.0844287.1700.1010287.200031.1065287.2100.1231287.240031.1286287.2500.1452287.280031.1507287.2900	.7105 286.4900 30.7159 286.5000 30.7214 .7324 286.5300 30.7379 286.5400 30.7433 .7543 286.5700 30.7598 286.6200 30.7872 .7982 286.6500 30.8037 286.6600 30.8092 .8201 286.6900 30.8256 286.7000 30.8311 .8421 286.7300 30.8476 286.7400 30.8531 .8641 286.7700 30.8696 286.7800 30.8751 .8861 286.8100 30.8916 286.8200 30.9191 .9301 286.8500 30.9136 286.8600 30.9191 .9301 286.8900 30.9356 286.9400 30.9631 .9741 286.9700 30.9796 286.9800 30.9851 .9962 287.0400 31.0182 287.0500 31.0237 .0347 287.0400 31.0403 287.0900 31.0458 .0568 287.1200 31.0623 287.1300 31.0678 .0789 287.1600 31.0844 287.1700 31.1120 .1231	.7324 286.530030.7379 286.540030.7433 286.5500.7543 286.570030.7598 286.580030.7653 286.5900.7762 286.610030.7817 286.620030.7872 286.6300.7982 286.650030.8037 286.660030.8092 286.6700.8201 286.690030.8256 286.700030.8311 286.7100.8421 286.730030.8476 286.740030.8531 286.7500.8641 286.770030.8696 286.780030.8751 286.7900.8861 286.810030.8916 286.820030.8971 286.8300.9081 286.850030.9136 286.860030.9191 286.8700.9521 286.930030.9576 286.940030.9411 286.9100.9521 286.970030.9796 286.980030.9851 286.9900.9962 287.000030.9962 287.010031.0017 287.0200.0127 287.040031.0182 287.050031.0237 287.0600.0347 287.080031.0403 287.090031.0458 287.1000.0568 287.120031.0844 287.170031.0899 287.1800.1010 287.200031.1065 287.210031.1120 287.2200

APPENDIX D. AUXILIARY PROGRAM (SEARAD CODE)

A. INTRODUCTION

"SEARAD" is a FORTRAN computer code that predicts the radiance (brightness) of the ocean surface. SEARAD" is valid for a spectral range extending from the visible to the far infrared regime. It is a self-contained, DOS-compatible program that runs on a personal computer and calculates sea radiance. It is a modified version of the Air Force program MODTRAN2 code that predicts sea radiance between 52.63 and 25000 cm⁻¹. MODTRAN is a computer code designed to determine atmospheric transmission and radiance at moderate resolution from 0 to 50,000 cm⁻¹. SEARAD is based on the Cox-Munk (Cox and Munk, 1954,1956) statistical model for wind-driven capillary wave facets. Preliminary comparisons show that SEARAD agrees to within several °C with actual sea radiance measurements in the mid-wave and long-wave in the infrared band. [Ref.1]

B. UNZIP SEARAD (INSTALLATION)

The following statement tells how to unzip and run "SEARAD". The zipped files span three disks altogether. The last disk will be disk 3; the first disk will be disk 1. These commands assume that the hard disk in the computer is drive c:, and that the 3 1/2 inch disks will be loaded into drive a:. If another drive is used instead for the 3 1/2 disks, the drive letter (b: for example) should be substituted for a: in the following instructions.

Sentences in parentheses are physical acts; sentences without parentheses are commands that should be typed on the keyboard.

To unzip:

c:\ mkdir searad
cd searad (Insert disk1 in drive a:)
copy a:\pkunzip.exe
pkunzip a:\source

```
pkunzip a:\input
pkunzip a:\exe (Follow instructions for disk insertion.)

The files should all be unzipped at this point. The directory c:\searad should now contain:
    zip utility: pkunzip.exe
    source code: Modnn [nn=10 to 22] (except mod21.for)
    Input file: Tape5xxx.std
    Log of mods: Note.txt
    Executables: Searad.exe, Dirac, and DOSxmsf.exe

To run Searad:
    copy tape5rad.std tape5
    searad
    type out
```

This should show the output file corresponding to the input file "Tape5rad.std ".[Ref.5]

C. SEARAD SAMPLE DESCRIPTION

In this section an example is provided to show how to use SEARAD to predict ocean radiance. An input file called "Tape5rad.std" employs a 1976 U.S. standard atmosphere to calculate ocean radiance observed at a zenith angle of 100 degree from a height of 23 m. The Navy aerosol model is used. The calculation is done with multiple scattering at low spectral resolution (LOWTRAN 7) for a single wave number (945 cm⁻¹) in the long wave band. The following DOS commands will calculate ocean radiance and print results

```
copy tape5rad.std tape5
searad
type out
```

These commands produce an output file called "out". The four contributions to ocean radiance (path to footprint, sea emission, sky reflection, and sun glint) are listed at the end of the "out" file. "TBOUND" in the input file here is interpreted as sea temperature.

D. SEARAD MODEL

The SEARAD model computes four contributions to sea radiance. The assumption for the model is that the strength of interaction between an optical ray and a capillary wave facet is given by the facet area projected normal to the ray. It does not include multiple reflections, shadowing and gravity waves. It also ignores polarization.

The first contribution is path radiance (N_{path}) . The footprint of a single pixel in an image of the sea is indicated by the wavy line. The footprint is observed by a receiver at the end of a ray whose zenith angle at the footprint is θ_r . N_{path} represents the spectral radiance in W/m²/sr/cm along the path from the footprint to the receiver.

The second contribution is reflected sky radiance $(N_{\rm sky})$. The spectral radiance $N_{\rm s}$ from part of the sky reaches the footprint along a ray whose zenith angle is $\theta_{\rm s}$. The contributions are the summation from all portions of the sky after specular reflection by the appropriate facets within the footprint. $N_{\rm sky}$ is the sum leaving the footprint at zenith angle $\theta_{\rm S}$. During its path to the receiver, $N_{\rm sky}$ is attenuated by the path transmission $\tau_{\rm path}$.

The third contribution is reflected solar radiance ($N_{\rm sun}$), sun glint. The radiance N_0 from the solar center arrives at the footprint along a path whose zenith angle is $\theta_{\rm o}$. Within the footprint most facets deflect the solar ray away from the receiver and are rejected, but some facets are retained because they deflect the ray specularly toward the receiver along a path with zenith angle θ_r . $N_{\rm sun}$ is the spectral radiance leaving the footprint after summation over rays arriving from all portions of the solar disk. $N_{\rm sun}$ is also attenuated by the path transmission $\tau_{\rm path}$.

The fourth contribution is thermal black body emission ($N_{\rm sea}$). In this portion each facet emits a spectral radiance $N_{\rm bb}$ given by Planck's equation for a black body. The sea temperature is equal to the value of TBOUND in the input file. The spectral emissivity of a given facet in the direction of the receiver is specified by the slope of that facet and the value of $\theta_{\rm r}$. $N_{\rm sea}$ is the thermal spectral radiance leaving the footprint for the

receiver after summation over all facets within the footprint. N_{sea} is also attenuated by path transmission τ_{path} after leaving the footprint.

The symbol ρ represents the reflectivity of sea water. It is calculated from Fresnel's equations. The total spectral radiance $N(\nu)$ received at wave number ν (cm⁻¹) is given by

$$N(v) = N_{path}(v)f(v) + \left[N_{sky}(v) + N_{sun}(v) + N_{sea}(v)\right]\tau_{path}(v)f(v) , \qquad (C.1)$$

where f(v) stands for the spectral responsivity of the receiver.

The design of SEARAD is such that the path (N_{path}, τ_{path}) and source (N_S, N_O, N_{bb}) values are taken from the original MODTRAN 2 while Fresnel reflection (ρ) and slope integrated values $(N_{sky}, N_{sun}, N_{sea})$ are introduced in new subroutines. Integration of Equation (C.1) over the wave number band specified in the input file (Tape5) is implemented in a modification of subroutine "TRAN" to produce the band integrated values for sea radiance given in the output file (out).[Ref.1]

APPENDIX E. DESCRIPTION OF EACH CARD IN SEARAD INPUT FILE

The format of input file is very important. Each number must be in the correct row and column. Below is a listing of the input file parameters in SEARAD and the values used in evaluating the sea radiance.

CARD 1 (line one)

- $F \Rightarrow use LOWTRAN 7$
- 7 ⇒ MODEL : radiosonde data used
- $3 \Rightarrow ITYPE : slant path to space$
- 1 ⇒ IEMSCT : program execution in radiance mode
- 1 ⇒ IMULT: program executed with multiple scattering
 "M1,M2,M3" are used to modify or supplement the altitude profiles of temperature and pressure, water vapor, and ozone "M4,M5,M6"
- $6 \Rightarrow M1$: default temperature and pressure to specified MODEL atmosphere (M1=1~6)
- $6 \Rightarrow M2 : default H₂O to specified MODEL atmosphere (M2=1~6)$
- $6 \Rightarrow M3 : default ozone to specified MODEL atmosphere (M3=1~6)$
- $6 \Rightarrow M4 : default CH4 to specified MODEL atmosphere (M4=1~6)$
- 6 \Rightarrow M5 : default N₂O to specified MODEL atmosphere (M5=1~6)
- 6 \Rightarrow M6: default CO to specified MODEL atmosphere (M6=1~6)
- 1 ⇒ MDEF use default profile for CO2, O2, NO, SO2, NO2, NH3, HNO3
- $1 \Rightarrow IM : radiosonde data to be read initially$
- 1 ⇒ NORPT : minimize printing of transmittance
- $xx \Rightarrow TBOUND : boundary temperature (0k)$
- $0.00 \Rightarrow SALB$: surface albedo (0.0 to 1.0)

```
CARD 2 (line 2)
3
      ⇒ IHAZE : navy maritime extinction, sets own VIS.
0
      ⇒ ISEASN : Summer for model 7
0
      ⇒ IVULCN : default to stratospheric background
3
      ⇒ ICSTL : air mass (1 for open ocean - 10 for strong continental
                   influence) ICSTL now allow non-integer values. Integers from
                   1 to 10 inclusive will be taken as is, while integers from 11 to 300
                   inclusive will be divided by 10. Integers outside the range of 1 to
                   300 will be reset to a default value of "3.0".
     ⇒ ICLD : no clouds or rain
0
     \Rightarrow IVSA : not used
20
     ⇒ VIS : meteorological range
1.897⇒ WSS: specifies current wind speed (m/s)
1.603⇒ WHH: 24 hour average wind speed (m/s)
0.00 \Rightarrow RAINT : rain rate (mm/hr)
0.00 \Rightarrow \text{GNDALT} altitude of surface relative to sea level (km)
CARD 2c (line 3)
      ⇒ ML : number of atmospheric layers to be inserted (Maximum of 34)
      ⇒ IRD1 : no read
      ⇒ IRD2 : no read
text TITLE: user defined text
CARD 2c1 (next 33 line)
      \Rightarrow ZMDL : altitude of layer (km)
\mathbf{X}\mathbf{X}
      \Rightarrow P: pressure at layer (mb)
```

 $\mathbf{X}\mathbf{X}$

 $\mathbf{X}\mathbf{X}$

 \Rightarrow T ambient temperature ($^{\circ}$ C)

```
⇒ JCHAR(RH) : relative humidity (%)
ABH \Rightarrow \text{ set units for P,T,RH}
CARD 3 (line 37)
0.006⇒ H1: initial altitude (FLIR sensor altitude) (km)
0.00 \Rightarrow H2: final altitude (seasurface altitude) (km)
    ⇒ ANGLE : zenith angle ( degree )
0.000 \Rightarrow RANGE : path length (km)
0.000 BETA: earth center angle subtented by H1 and H2 (degree)
0.000⇒ RO : default radius of earth (km)
     ⇒ LEN for long path through tangent height
90.00⇒ Psi: azimuth of the upwind direction from line of sight positive East of North
               (degree) 90 ° means that the wind is blowing from right to left,
               perpendicular to the direction of observation
         True: sea radiance will be carried out (F means that sea radiance will be
T
                   prevented under all conditions)
CARD 4 (line 38)
830 \Rightarrow V1: initial wave number (cm<sup>-1</sup>)
1250 \Rightarrow V2: final wave number (cm<sup>-1</sup>)
10
      ⇒ DV : wave number increment ( cm<sup>-1</sup> )
2
      ⇒ filter
CARD 5
0
      ⇒ IRPT : end program (3 means read CARD 3 again)
```

APPENDIX F. SEARAD INPUT DATA

EOMET95 Data Set from NPS Boundary Layer Meteorology Group

Header Entries form Appendix E

F	7 3	1 1	6 6	6 6	6 6	1 1	1	206 60	0 00
-	3 0	0 3	0 0	10.000	1.897	1.603		286.60 000	0.00 .000
	33 0		L:37:53 MAY		1.057	1.005	. 0	100	.000
	0.003	1013.400	12.100	90.0		AB:	u		
	0.017	1011.700	13.300	70.0		AB			
	0.021	1011.300	13.000	72.0		AB			
	0.031	1010.100	12.900	74.0		'AB			
	0.042	1008.800	12.800	75.0		AB			
	0.046	1008.300	12.800	76.0		AB			
	0.056	1007.100	12.600	77.0		AB			
	0.070	1005.300	12.500	78.0		AB			
	0.075	1004.900	12.500	78.0		AB:	Н		
	0.083	1003.900	12.500	77.0	•	AB:	H		
	0.093	1002.600	12.500	75.0		AB:	H	•	
	0.103	1001.400	12.500	74.0		AB:	H		
	0.113	1000.200	12.500	73.0	•	AB:	H ·		
	0.119	999.500	12.400	73.0		AB:			
	0.128	998.500	12.400	73.0		AB:			
	0.137	997.400	12.500	73.0		AB:			
	0.150	995.800	12.500	73.0		AB:		•	
	0.153	995.500	12.700	72.0		AB			
	0.160	994.600	12.800	70.0		AB:			
	0.164	994.100	12.800	70.0		AB:			
	0.185 0.190	991.700	12.800	69.0		AB:			
	0.190	991.100 989.800	12.800	69.0 69.0		AB:			
	0.201	988.900	12.800 12.700	69.0		AB:			
	0.208	987.800	12.700	69.0		AB: AB:			
	0.228	986.600	12.600	69.0		AB:			
	0.234	985.900	12.500	69.0		AB:			
	0.244	984.700	12.400	69.0		AB:			
	0.256	983.300	12.300	68.0		AB			
	0.266	982.100	12.300	69.0		AB			
	0.275	981.100	12.100	69.0		AB			
	0.283	980.100	12.100	69.0		AB			
	0.291	979.200	12.100	69.0		AB			
	0.006	0.000	90.240	.000	.000	0.00	1	252.00	0 Т
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F	7 3	1 1	6 6	6 6	6 6	1 1	1	286.60	0.00
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	33 0		ypical case	:					
	0.003	1013.400	12.100	90.0					
	0.017	1011.700	13.300	70.0		AB	H		
	0.021	1011.300	13.000	72.0		AB	H		
	0.031	1010.100	12.900	74.0		AB	H		
	0.042	1008.800	12.800	75.0		AB	H		
	0.046	1008.300	12.800	76.0		AB.	H		
	0.056	1007.100	12.600	77.0		AB.	H		
	0.070	1005.300	12.500	78.0		AB	H		
	0.075	1004.900	12.500	78.0		AB	H		
	0.083	1003.900	12.500	77.0		AB.	H		
	0.093	1002.600	12.500	75.0		AB:	H		
	0.103	1001.400	12.500	74.0		AB:	H		
	0.113	1000.200	12.500	73.0		AB.	H		
	0.119	999.500	12.400	73.0		AB:	H		
	0.128	998.500	12.400	73.0		AB:	H		•
	0.137	997.400	12.500	73.0		AB:	H		
	0.150	995.800	12.500	73.0		AB	H		
	0.153	995.500	12.700	72.0		AB	H		
	0.160	994.600	12.800	70.0		AB	H		
	0.164	994.100	12.800	70.0		AB	H		
	0.185	991.700	12.800	69.0		AB	H		
	0.190	991.100	12.800	69.0		AB			
	0.201	989.800	12.800	69.0		AB			
	0.208	988.900	12.700	69.0		AB			
	0.218	987.800	12.600	69.0		AB			
	0.228	986.600	12.600	69.0		AB			
	0.234	985.900	12.500	69.0		ABI			
	0.244	984.700	12.400	69.0		ABI			
	0.256	983.300	12.300	68.0	•	, ABI			
	0.266	982.100	12.300	69.0		ABI			
	0.275	981.100	12.100	69.0		ABI			
	0.283	980.100	12.100	69.0		ABI			
	0.291	979.200	12.100	69.0	000	ABI		050 00	
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	0.017	1011.700	13.000	70.0		ABI		
	0.021	1010.100	12.900	72.0 74.0		ABI		
	0.031	1008.800	12.800	75.0		ABI		
	0.042	1008.300	12.800	76.0		ABI		
	0.056	1003.300	12.600	77.0		ABI		
	0.030	1007.100	12.500	78.0		ABI		
	0.075	1003.300	12.500	78.0		ABI		
	0.083	1004.900	12.500	77.0		ABI		
	0.093	1003.500	12.500	75.0		ABI ABI		
	0.103	1001.400	12.500	74.0		ABI		
	0.113	1000.200	12.500	73.0		ABI		
	0.119	999.500	12.400	73.0		ABI		
	0.128	998.500	12.400	73.0		ABI		
	0.137	997.400	12.500	73.0		ABI		
	0.150	995.800	12.500	73.0		ABI		
	0.153	995.500	12.700	72.0		ABI		
	0.160	994.600	12.800	70.0		ABI		
	0.164	994.100	12.800	70.0		ABI		
	0.185	991.700	12.800	69.0		ABI		
	0.190	991.100	12.800	69.0	•	ABI		
	0.201	989.800	12.800	69.0		ABI		
	0.208	988.900	12.700	69.0		ABI		
	0.218	987.800	12.600	69.0		ABI	H	
	0.228	986.600	12.600	69.0		ABI	H	
	0.234	985.900	12.500	69.0		ABI	H	
	0.244	984.700	12.400	69.0		ABI	H	
	0.256	983.300	12.300	68.0		ABI	H	
	0.266	982.100	12.300	69.0		ABI		
	0.275	981.100	12.100	69.0		ABI		
	0.283	980.100	12.100	69.0		ABI		
	0.291	979.200	12.100	69.0		ABI		
	0.250	0.000	95.000	.000 .	.000	0.00	1 252	т 000.
	830	1250	10	1				

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7
F
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    3
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                    3
                                   10.000
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                                                        1.603
                                                                    .000
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   33
         0
              0
                   MDR Estimate-2
     0.003 1013.400
                         12.100
                                     90.0
                                                               ABH
     0.017
            1011.700
                         13.300
                                     70.0
                                                              ABH
     0.021
            1011.300
                         13.000
                                     72.0
                                                              ABH
     0.031
            1010.100
                         12.900
                                     74.0
                                                              ABH
     0.042
            1008.800
                         12.800
                                     75.0
                                                              ABH
            1008.300
     0.046
                         12.800
                                     76.0
                                                              ABH
     0.056
            1007.100
                         12.600
                                     77.0
                                                              ABH
     0.070
           1005.300
                         12.500
                                     78.0
                                                              ABH
     0.075
            1004.900
                         12.500
                                     78.0
                                                              ABH
     0.083
            1003.900
                         12.500
                                     77.0
                                                              ABH
            1002.600
     0.093
                         12.500
                                     75.0
                                                              ABH
     0.103
            1001.400
                         12.500
                                     74.0
                                                              ABH
            1000.200
                         12.500
                                     73.0
     0.113
                                                              ABH
     0.119
             999.500
                         12.400
                                     73.0
                                                              ABH
     0.128
             998.500
                         12.400
                                     73.0
                                                              ABH
     0.137
             997.400
                         12.500
                                     73.0
                                                              ABH
     0.150
             995.800
                         12.500
                                     73.0
                                                              ABH
     0.153
             995.500
                        12.700
                                     72.0
                                                              ABH
     0.160
             994.600
                         12,800
                                     70.0
                                                              ABH
             994.100
     0.164
                        12.800
                                     70.0
                                                              ABH
     0.185
             991.700
                        12.800
                                     69.0
                                                              ABH
     0.190
             991.100
                        12.800
                                     69.0
                                                              ABH
     0.201
             989.800
                        12.800
                                     69.0
                                                              ABH
     0.208
             988.900
                        12.700
                                     69.0
                                                              ABH
     0.218
             987.800
                         12.600
                                     69.0
                                                              ABH
                        12.600
     0.228
             986.600
                                     69.0
                                                              ABH
     0.234
             985.900
                        12.500
                                     69.0
                                                              ABH
     0.244
             984.700
                        12.400
                                     69.0
                                                              ABH
     0.256
             983.300
                        12.300
                                     68.0
                                                              ABH
     0.266
             982.100
                        12.300
                                     69.0
                                                              ABH
     0.275
             981.100
                        12.100
                                     69.0
                                                              ABH
     0.283
             980.100
                        12.100
                                     69.0
                                                              ABH
     0.291
             979.200
                         12.100
                                     69.0
                                                              ABH
     0.250
              0.000
                         90.550
                                     .000
                                                .000
                                                          0.00 1
                                                                       252.000
                                                                                  Т
       830
                1250
                            10
```

APPENDIX G. SEARAD OUTPUT DATA

**** SEARAD, A MODIFICATION OF LOWTRAN7 *****

DATE: 11/21/1997 TIME: 12:00:50.69

THERMAL RADIANCE MODE

MULTIPLE SCATTERING USED

MARINE AEROSOL MODEL USED

WIND SPEED =

1.90 M/SEC 1.60 M/SEC, 24 HR AVERAGE WIND SPEED =

RELATIVE HUMIDITY = 89.93 PERCENT

AIRMASS CHARACTER = 3

VISIBILITY 10.00 KM

SLANT PATH TO SPACE

.006 KM .000 KM Н1 = HMIN = ANGLE 90.240 DEG =

FREQUENCY RANGE

IV1 830 CM-1 (12.05 MICROMETERS) IV2 1250 CM-1 (8.00 MICROMETERS) IDV 10 CM-1 IFWHM 1 CM-1 IFILTER =

SUMMARY OF THE GEOMETRY CALCULATION

.006 KM H1 .000 KM H2 ANGLE === 90.240 DEG RANGE == 1.444 KM BETA .013 DEG PHI89.764 DEG MIMH == .000 KM BENDING = .009 DEG LEN

SEA AT 286.60 K REPLACES BLACK BODY BOUNDARY

UPWIND = 252.000 DEG EAST OF LINE OF SIGHT

ZERO RANGE VALUES

SEA EMISSION = 14.42182 W M-2 SR-1 (AV. EMISS.

.4636)

SKY REFLECTION = 5.22488 W M-2 SR-1 SUN GLINT .00000 W M-2 SR-1 TOTAL RADIANCE = 19.64670 W M-2 SR-1BLACK BODY TEMP. = -10.1 C

FULL RANGE VALUES

PATH TO FOOTPRINT = 7.95021 W M-2 SR-1 (AV. TRANS.

.7181)

 SEA EMISSION
 =
 10.50470 W M-2 SR-1

 SKY REFLECTION
 =
 3.70776 W M-2 SR-1

 SUN GLINT
 =
 .00000 W M-2 SR-1

TOTAL RADIANCE = 22.16267 W M-2 SR-1BLACK BODY TEMP. = -4.3 C

**** SEARAD, A MODIFICATION OF LOWTRAN7 ****

DATE: 11/21/1997 TIME: 12:03:37.72 THERMAL RADIANCE MODE MULTIPLE SCATTERING USED MARINE AEROSOL MODEL USED 1.90 M/SEC 1.60 M/SEC, 24 HR AVERAGE WIND SPEED = WIND SPEED = RELATIVE HUMIDITY = 89.93 PERCENT AIRMASS CHARACTER = 3 VISIBILITY 10.00 KM SLANT PATH TO SPACE .006 KM H1 HMIN == 90.043 DEG = ANGLE FREQUENCY RANGE IV1 830 CM-1 (12.05 MICROMETERS) = 1250 CM-1 (8.00 MICROMETERS) IV2 = IDV 10 CM-1 = IFWHM = 1 CM-1 IFILTER = SUMMARY OF THE GEOMETRY CALCULATION H1 .006 KM H2 .291 KM -ANGLE 90.043 DEG = RANGE = 97.261 KM BETA = .875 DEG PHI = 90.487 DEG .000 KM HMIN BENDING = .344 DEG 1 TBOUND SET TO .10 K FOR MARINE SKY INTEGRATED ABSORPTION = 420.00 CM-1 FROM 830 TO 1250 CM-1 AVERAGE TRANSMITTANCE = .0000 MAXIMUM RADIANCE = 1.033E-01 W M-2 SR-1 (CM-1)-1 AT 830.0 CM-1MINIMUM RADIANCE = 4.248E-02 W M-2 SR-1 (CM-1)-1 AT 1250.0 CM-1 BOUNDARY TEMPERATURE = .10 K BOUNDARY EMISSIVITY = 1.000 FILTERED RADIANCE = 2.904E+01 W M-2 SR-1BLACKBODY TEMPERATURE = 9.8 C

**** SEARAD, A MODIFICATION OF LOWTRAN7 ****

DATE: 11/21/1997 TIME: 12:06:44.19

THERMAL RADIANCE MODE

MULTIPLE SCATTERING USED

MARINE AEROSOL MODEL USED

WIND SPEED

= 1.90 M/SEC = 1.60 M/SEC, 24 HR AVERAGE WIND SPEED = 1.90 M/SEC WIND SPEED = 1.60 M/SEC, 2 RELATIVE HUMIDITY = 89.93 PERCENT AIRMASS CHARACTER = 3

VISIBILITY 10.00 KM

SLANT PATH TO SPACE

.250 KM H1 HMIN = 95.000 DEG ANGLE =

FREQUENCY RANGE

830 CM-1 (12.05 MICROMETERS) IV1 IV2 = 1250 CM-1 (8.00 MICROMETERS) IDV = 10 CM-1 = IFWHM 1 CM-1 IFILTER =

SUMMARY OF THE GEOMETRY CALCULATION

.250 KM H1 Н2 = .000 KM 95.000 DEG ANGLE = RANGE = 2.875 KM BETA .026 DEG 85.020 DEG PHI .000 KM HMIN = .006 DEG BENDING = LEN = 0

SEA AT 286.60 K REPLACES BLACK BODY BOUNDARY

UPWIND = 252.000 DEG EAST OF LINE OF SIGHT

ZERO RANGE VALUES

= 18.29033 W M-2 SR-1 (AV. EMISS. SEA EMISSION

.5882)

SKY REFLECTION = 3.71435 W M-2 SR-1 SUN GLINT = .00000 W M-2 SR-1

TOTAL RADIANCE = 22.00468 W M-2 SR-1

BLACK BODY TEMP. -4.7 C

FULL RANGE VALUES

.6154)	PATH TO FOOTPRINT	=	10.91463 W M-2 SR-1 (AV. TRANS.
,	SEA EMISSION SKY REFLECTION SUN GLINT	=	11.46502 W M-2 SR-1 2.24949 W M-2 SR-1 .00000 W M-2 SR-1
	TOTAL RADIANCE BLACK BODY TEMP.	=	24.62915 W M-2 SR-1 1.1 C

***** SEARAD, A MODIFICATION OF LOWTRAN7 *****

DATE: 11/21/1997 TIME: 12:09:01.17

THERMAL RADIANCE MODE

MULTIPLE SCATTERING USED

MARINE AEROSOL MODEL USED

WIND SPEED =

1.90 M/SEC 1.60 M/SEC, 24 HR AVERAGE = WIND SPEED

RELATIVE HUMIDITY = 89.93 PERCENT

AIRMASS CHARACTER = 3

VISIBILITY 10.00 KM

SLANT PATH TO SPACE

.250 KM H1 HMIN .000 KM ANGLE 90.550 DEG

FREQUENCY RANGE

IV1 830 CM-1 (12.05 MICROMETERS) IV2 = 1250 CM-1 (8.00 MICROMETERS) IDV = 10 CM-1 IFWHM = 1 CM-1 IFILTER =

SUMMARY OF THE GEOMETRY CALCULATION

.250 KM Н1 = Н2 .000 KM = ANGLE = 90.550 DEG RANGE = 33.415 KM .300 DEG BETA = = 89.683 DEG PHI = HMIN .000 KM BENDING = .067 DEG LEN

SEA AT 286.60 K REPLACES BLACK BODY BOUNDARY

UPWIND = 252.000 DEG EAST OF LINE OF SIGHT

ZERO RANGE VALUES

= 14.46294 W M-2 SR-1 (AV. EMISS. SEA EMISSION

.4649)

SKY REFLECTION = 5.26282 W M-2 SR-1 SUN GLINT = .00000 W M-2 SR-1

TOTAL RADIANCE = 19.72575 W M-2 SR-1

BLACK BODY TEMP. = -9.9 C

FULL RANGE VALUES

.0171)	PATH TO FOOTPRINT	=	28.50598	W M-2	SR-1	(AV. TRANS.
,	SEA EMISSION SKY REFLECTION SUN GLINT	=======================================	.07884	W M-2	SR-1	
	TOTAL RADIANCE BLACK BODY TEMP.	=	28.82764 9.5		SR-1	

APPENDIX H. GPS DATA

Source: EOMET95 Data Set

ws: wind speed ta: air temperature

ts: sea temperature lon: longitude

lat: latitude

shs: ship seep rh: relative humidity

shd: ship direction pr: pressure

wd: wind direction

sid. sinp direction		CHOII	pr. pressure								
date	time	ws	wd	ta	rh	pr	shs	shd	lat	lon	ts
950515	2030	1.00	153	14.55	70.40	1010	0.01	264	36 80	-121.79	16.90
950515	2040	0.45	204	13.98	72.84		0.02	30	36.80	-121.79	16.50
950515	2050	0.01	309	14.22	72.70		0.02	48		-121.79	17.60
950515	2100	0.64	243	15.02	69.92		0.01	300		-121.79	18.20
950515		0.24	274	15.74	70.76		0.05	37		-121.79	19.10
950515	2120	2.14	275	16.28	68.09		1.24	340		-121.79	14.20
950515		5.17	240	14.77	76.57	1010	4.77	247		-121.80	12.30
950515		4.25	248	13.91	82.30	1011	5.11	254		-121.83	13.10
950515		6.64	258	13.06	87.38		4.84	257		-121.87	13.40
950515		6.12	261	13.05	87.31	1011	4.71	256		-121.90	12.40
950515		6.09	274	13.19	85.85		4.56	254	36.78	-121.93	12.30
950515		5.66	289	13.01	86.30		4.53	250	36.77	-121.96	12.70
950515		5.46	299	13.07	83.25		4.46	250	36.76	-121.98	13.00
950515		4.68	304	13.30	81.02		2.59	257		-122.01	13.50
950515		3.94	300	13.52	82.33		0.50	275.		-122.02	13.80
950515		2.98	298	13.48	84.72		0.51	282		-122.02	13.90
950515		2.68	302	13.40	84.98		0.59	284		-122.02	13.90
950515		2.62	314	13.47	84.37		0.58	279		-122.03	13.90
950515 950515		2.74 2.90	331	13.53	84.75		0.59	280		-122.03	13.90
950515		3.00	308 294	13.54	85.24		0.55	291		-122.04	14.10
930313	2350	3.00	294	13.48	86.07	1011	0.49	293	36.76	-122.04	13.90
950516	0	3.01	276	13.23	88.50	1010	0.48	268	36 76	-122.04	13.80
950516	10	3.84	279	12.94	89.52		0.48	258		-122.05	13.70
950516	20	4.68	287	12.79	88.76		0.50	245		-122.05	13.60
950516	30	4.67	296	12.73	88.49		0.47	264		-122.05	13.80
950516	40	3.39	316	12.80	90.10		0.51	281		-122.06	13.80
950516	50	2.84	307	12.90	89.16		0.48	273		-122.06	13.90
950516	100	2.56	304	13.03	88.12		0.51	284		-122.06	13.80
950516	110	2.97	279	12.90	89.18	1010	0.47	280		-122.06	13.70
950516	120	3.31	277	12.79	89.80	1010	0.47	275		-122.07	13.60
950516	130	2.20	270	12.76	89.59		0.50	268	36.76	-122.07	13.40
950516	140	2.75	284	12.84	88.16		0.52	273	36.76	-122.07	13.50
950516	150	2.39	292	12.87	88.92		0.55	274		-122.08	13.30
950516	200	3.15	290	12.82	87.96			258		-122.08	13.20
950516	210	3.35	284	12.79	88.42		0.64	261		-122.09	13.10
950516	220	3.27	278	12.79	89.44		0.60	264		-122.09	13.00
950516	230	2.70	275	12.73	90.49		0.67	269		-122.10	12.80
950516	240	2.62	259	12.74	91.73		0.89	241		-122.10	12.80
950516 950516	250	1.90	259	12.79	91.96		1.00	242		-122.11	13.10
950516	300 310	2.34 3.64	206 207	12.81	91.82		1.05	242		-122.11	13.20
950516	320	4.18	207	12.69 12.72	91.33		0.78	249		-122.12	12.90
950516	330	3.89	190	12.72	90.70 89.32		0.79 0.75	249 243	36.75	-122.12	12.80
950516	340	4.13	207	12.74	88.34		0.75	243 251	36.75	-122.13 -122.13	13.00
20010	. 540	4.13	201		00.34	TOTT	0.70	231	30.74	-122.13	13.10

```
950516 420
                   3.23
                          244 12.82 89.98 1011
                                                           0.82 254
                                                                           36.74 -122.15 13.40
                                                          0.76 255
0.78 254
0.81 261
                                          90.73 1011
                                                                          36.74 -122.16 13.50
950516
                                 12.77
           430
                   3.52
                          245
                                                                          36.74 -122.16
36.74 -122.17
36.74 -122.17
950516
           440
                   3.45
                          252
                                 12.77
                                          90.58 1011
                                                                                               13.40
                                          90.53 1011
950516
                  3.09
                                 12.72
           450
                          264
                                                                                               13.30
                                                           0.88 259
950516
           500
                  2.90
                          263
                                 12.72
                                          90.76 1011
                                                                                               13.20
950516
           510
                  2.83
                          254
                                12.67
                                          91.26 1011
                                                           0.90
                                                                  262
                                                                          36.73 -122.18
                                                                                               13.10
950516
          520
                  2.98
                          245
                                12.66 92.01 1011
                                                           0.91
                                                                   265
                                                                          36.73 -122.18
950516
                  2.07
                                12.62
12.59
                                                                          36.73 -122.19
          530
                          254
                                          92.70 1011
                                                           0.88
                                                                   263
                                                                                               13.10
                                                           0.92 260 36.73 -122.20
0.97 261 36.73 -122.20
0.94 257 36.73 -122.21
0.77 247 36.73 -122.21
950516 540
                  2.32
                          261
                                          93.39 1012
                                                                                               13.10
950516 550
                                12.58
                                          93.88 1012
                  2.66
                          279
                                                                                               13.00
950516 600
                  2.48
                          279
                                12.55
                                          94.00 1012
                                                                                              12.90
950516 610
                  1.79 308 12.55
                                          94.07 1011
                                                                                              12.90
                                                           0.77 247 36.73 -122.21

0.80 253 36.73 -122.22

0.83 251 36.73 -122.22

0.82 258 36.73 -122.23

0.81 258 36.72 -122.23

0.77 259 36.72 -122.24

0.79 262 36.72 -122.24
950516
          620
                  1.67
                          318 12.49
                                          94.98 1011
                                12.36
12.26
                                          95.72 1011
950516
                  1.96 358
           630
                                                                                              13.00
950516
                                                                                              13.00
12.90
           640
                  2.18
                           36
                                          95.94 1011
                          53 12.20
950516
           650
                  1.51
                                          95.95 1011
                          61 12.14
950516
                                                                                              12.80
          700
                  1.45
                                          96.00 1011
                          39 12.19 96.02 1011
950516 710
                  2.11
                                                                                              12.90
950516 720
                  2.53
                          3 12.23 96.02 1011
                                                           0.78 262 36.72 -122.25
                                                                                              13.00
                                                          0.78 262 36.72 -122.25 13.00

0.73 256 36.72 -122.26 13.10

0.77 254 36.72 -122.26 13.30

0.77 254 36.72 -122.26 13.30

0.74 251 36.72 -122.27 13.10

0.74 252 36.72 -122.27 13.00

0.76 253 36.72 -122.28 13.00

0.78 268 36.71 -122.28 13.00
950516
          730
                  2.68 338 12.30 96.11 1011
                          332 12.42 96.05 1011
7 12.38 94.99 1011
343 12.45 94.50 1011
950516
          740
                  2.29
950516
          750
                  3.23
950516 800
                  3.68
                          344 12.44 94.11 1011
                  3.83
950516 810
950516
                  3.65
                          354 12.37 94.90 1011
          820
                                                          0.78 268 36.71 -122.28 13.00

0.79 266 36.71 -122.29 13.00

0.81 258 36.71 -122.30 13.10

0.79 261 36.71 -122.30 13.10

0.87 261 36.71 -122.31 13.00
950516
                  3.53
                          22 12.27 95.60 1011
          830
                          25 12.13 95.98 1011
950516
          840
                  3.63
                                12.09
950516
          850
                  3.88
                           21
                                          96.23 1011
                           31 12.04 96.50 1011
950516
          900
                  4.18
950516
                          53 11.86 96.91 1011
          910
                  4.53
950516 920
                  4.45
                          47 11.81 97.61 1011
                                                          0.89 252 36.71 -122.31
                                                                                              13.00
                          47 11.79 97.98 1011
57 11.75 98.04 1011
47 11.65 98.15 1011
67 11.69 98.54 1011
950516 930
                  3.56
                                                          0.64 260 36.71 -122.32
                                                                                               13.00
                                                          0.26 254 36.71 -122.32
1.00 251 36.71 -122.32
0.92 263 36.71 -122.33
0.78 263 36.71 -122.34
950516 940
950516 950
                  2.41
                                                                                               13.10
                                                                                              13.10
                  2.63
950516 1000
                  2.56
                                                                                               13.10
                          57 11.73 98.85 1011
950516 1010
                                                                                              13.10
                  1.68
950516 1020
                          54 11.76 98.98 1011
                                                          0.71 268 36.71 -122.34
                  1.72
                                                                                              13.20
                                                          0.73 269 36.71 -122.35 13.20
0.75 272 36.71 -122.35 13.20
0.77 269 36.71 -122.36 13.20
0.68 272 36.71 -122.36 13.20
950516 1030
                  1.70
                          65 11.80 98.99 1011
                                11.74 99.02 1011
11.79 99.02 1011
950516 1040
                  1.69
                           78
950516 1050
                          90
                  0.95
950516 1100
                          99 11.96 99.46 1011
                  0.91
950516 1110
                  1.23 104 12.13 99.65 1011
                                                          0.67 273 36.71 -122.36
                                                                                              13.30
950516 1120
                  0.59
                          88 12.12 99.16 1011
                                                          0.59 269 36.71 -122.37
                                                                                               13.20
                          76 11.96 99.06 1011
360 11.85 99.28 1011
355 11.83 99.74 1011
0 11.84 99.95 1011
1 11.80 100.00 1011
                                                                   270 36.71 -122.37
950516 1130
                  0.63
                                                          0.66
                                                                                               13.20
                                                          0.66 270 36.71 -122.38

0.60 271 36.71 -122.38

0.65 269 36.71 -122.39
950516 1140
950516 1150
                  1.30
                                                                                               13.10
                  2.03
                                                                                               13.20
950516 1200
                  2.17
                                                                                              13.20
                                                           0.59 267 36.71 -122.39 13.20
950516 1210
                  1.96
                                                          0.59 269 36.71 -122.39

0.60 271 36.71 -122.40

0.53 270 36.71 -122.40

0.49 270 36.71 -122.41
950516 1220
                  2.34
                          20 11.81 100.00 1011
950516 1230
950516 1240
                           44 11.80 100.02 1011
                  2.26
                                                                                              13.20
                  2.09
                           37
                                 11.64 100.02 1011
                                                                                               13.10
                           40 11.70 100.09 1011
950516 1250
                  2.42
                                                                                               13.10
950516 1300
                           56 11.60 100.07 1011
                                                                          36.71 -122.40
                  3.18
                                                           1.91
                                                                   74
                                                                                               13.20
950516 1310
                  3.29
                          73 11.58 99.71 1011
                                                           4.68
                                                                  78
                                                                          36.71 -122.38
                                                                                               13.30
950516 1320
950516 1330
                          61 11.43 98.70 1011
61 11.36 97.50 1011
74 11.38 96.42 1011
                                                                  77
                                                                          36.72 -122.35
                  2.15
                                                           4.68
                                                                                               13.10
                                                                           36.72 -122.32
36.73 -122.29
36.73 -122.25
                                                           4.76
                                                                    77
                                                                                              13.10
                  1.94
950516 1340
                  2.24
                                                           4.83
                                                                    80
950516 1350
                  2.70
                           83 11.40 95.96 1011
                                                           4.81
                                                                                              12.90
                                                                    81
950516 1400
                  1.72
                           79 11.31
                                         95.69 1011
                                                           4.74
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                                                                 36.80 -121.80
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0.97 167
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281 36.81 -121.81
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36.80 -121.79 21.60
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950518 1820
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11.51 89.09 1016
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                             11.79 88.67 1016
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0.01 260 36.80 -121.79 23.40
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950518 1900
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346 36.80 -121.79 24.50
170 36.80 -121.79 23.80
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0.01 346
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256 36.77 -121.95 12.70
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950518 2310
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950518	2350	4.96	275	11.34	90.02 1015	0.64	275	36.77 -122.01	13.20
950519 950519 950519 950519	0 10 20 30	4.73 4.82 4.67 3.60	277 283 277 286	11.26 11.18 11.13 11.11	90.69 1014 90.52 1014 91.13 1014 91.41 1014	0.76 0.72 0.70 0.74	254 252 262 274	36.77 -122.02 36.76 -122.02 36.76 -122.03 36.76 -122.03	13.10 13.10 13.20 13.10
950519 950519	40 50	4.24	307 293	11.10	92.00 1014 92.18 1014	0.67 0.74	285 292	36.76 -122.04	13.10
950519 950519	100 110	4.10	299	11.04	92.91 1014	0.74	290	36.77 -122.04 36.77 -122.05	13.10 12.90
950519	120	4.27 3.98	306 303	11.06 11.02	93.22 1014 93.52 1014	0.81 0.78	293 291	36.77 -122.05 36.77 -122.06	12.80 12.70
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950519 950519	150 200	3.95 3.88	283 272	11.07	93.68 1014	0.79	270	36.77 -122.07	13.10
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950519 950519	220 230	3.81 3.44	272 265	11.06 10.99	94.47 1014 95.27 1014	0.85 0.89	258 256	36.77 -122.09 36.77 -122.09	13.10 13.10
950519 950519	240 250	3.52 3.85	257 265	10.91 10.79	95.70 1014 96.01 1014	0.84 0.74	.262	36.77 -122.10	13.00
950519	300	2.98	276	10.65	96.44 1014	0.77	252 253	36.77 -122.10 36.77 -122.11	12.80 12.70
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950519 950519	330 340	4.04 3.76	272 276	10.72 10.68	97.47 1014 97.64 1014	0.70 0.75	256 246	36.76 -122.12 36.76 -122.13	12.80 12.70
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950519	410	4.28	297	10.62	98.00 1014 98.08 1014	0.70 0.77	252 244	36.76 -122.13 36.76 -122.14	12.70 12.70
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950519 950519	440 450	3.89 3.73	328 324	10.55 10.55	98.99 1014 98.50 1014	0.99 1.13	265 261	36.76 -122.15 36.75 -122.16	12.50 12.50
950519 950519	500 510	3.24	328 330	10.73	98.17 1014	1.11	256	36.75 -122.17	12.60
950519	520	3.19	331	10.91 10.95	97.93 1015 97.56 1015	1.13 1.13	249 247	36.75 -122.18 36.75 -122.18	12.60 12.70
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950519 950519	550 600	4.08 4.12	320 32 4	11.01 10.88	97.18 1014 97.25 1014	1.03 0.73	245 238	36.74 -122.20 36.74 -122.21	12.60 12.60
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950519	630	4.94	314	10.81	97.61 1014	0.79 0.77	239 233	36.74 -122.22 36.73 -122.22	12.60 12.60
950519 950519	640 650	4.74 4.42	316 315	10.94 10.98	97.17 1014 96.98 1014	0.70 0.82	235 223	36.73 -122.23 36.73 -122.23	12.60 12.60
950519 950519	700 710	5.10 4.81	315 317	11.00 11.10	96.58 1014 96.07 1014	0.76 0.62	227 235	36.73 -122.23 36.72 -122.24	12.60 12.70
950519 950519	720 730	3.83 4.21	312 325	11.09	96.18 1014 96.44 1014	0.77	223	36.72 -122.24	12.70
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950519 1920
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950519 2000
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950519		5.16	288	10.39 10.63	97.88 1013 96.90 1013	4.56 4.57	252 256	36.77 -121.93 36.76 -121.96	13.40
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950519		7.53	283	11.10	94.21 1012	0.56	268	36.74 -122.07	13.10
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950520	140	6.73	265	10.69	96.27 1012	0.73	255	36.73 -122.12 36.73 -122.12	13.10 13.10
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950520	200	6.46	273	10.73	97.13 1012	0.72	259	36.73 -122.13	13.10
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950520	230	6.17	279	10.46	97.14 1012	0.75	258	36.73 -122.14	12.90
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950520	300	5.92	270	10.52	96.81 1012	0.84	250	36.72 -122.16	12.70
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950520	400	5.73	296	10.28	95.86 1012	0.77	264	36.72 -122.19	12.50
950520	410	5.50	303	10.32	95.98 1013	0.79	262	36.72 -122.20	12.60
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950520	540 550	4.34	320	10.27 10.36	94.07 1013	$0.86 \\ 1.01$	267 260	36.71 -122.25	12.60
950520	600	4.34	318	10.36	94.29 1013	1.01	259	36.71 -122.25 36.71 -122.26	12.60 12.60
950520	610	4.88	312	10.46	93.97 1013	1.16	264	36.71 -122.27	12.60
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950521	530	4.83	316	12.20	79.21 1015	0.67	309	36.70 -122.38	13.20
950521	540	4.72	315	12.23	79.57 1015	0.60			
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950521	550	5.40	321	12.25	80.58 1015	0.60	327	36.71 <i>-</i> 122.39	13.30
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950521	610	4.97	323	12.19	77.81 1015	0.53	320	36.71 -122.39	13.30
950521	620	4.36	321	12.25	78.70 1015	0.55	308	36.71 -122.40	13.30
950521	630	4.48	319	12.27	80.16 1015	0.61	309	36.72 -122.40	13.30
950521	640	5.65	322	12.21	79.90 1015	0.56	319	36.72 -122.40	13.30
950521	650	4.15	322	12.24	78.02 1015	0.60	321	36.72 -122.40	13.30
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950521	710	4.80	325	12.17	78.39 1015	0.53	312	36.72 -122.41	13.40
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950521	920	3.96	326	12.08	77.53 1014	0.70	323	36.76 -122.44	13.30
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950522	2300	9.44	264	11.45	89.63 1013	0.42	253	36.76 -122.05	13.20
950522		9.12	256	11.41					
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950522	2330	8.19	255	11.45	87.36 1013	0.47	240	36.76 -122.06	13.30
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950522		8.77	255						
330322	2330	0.77	233	11.47	87.95 1013	0.50	238	36.75 -122.06	13.20
950523	0	9.30	252	11.44	87.96 1013	0.42	237	36.75 -122.07	13.20
950523	10	8.21	249	11.47	88.43 1013	0.35	234	36.75 -122.07	13.20
950523	20	9.53	246	11.43	88.09 1013	0.53	233	36.75 -122.07	13.20
950523	30	9.03	263	11.44	87.85 1013	0.58	250	36.75 -122.07	12.90
950523	40	8.46	264	11.51	87.82 1013	0.64	249	36.75 -122.08	12.90
950523	50	7.72	275	11.56	87.70 1013	0.59	267		
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950523	120	9.07	277	11.50	87.15 1013	0.72	272	36.75 -122.09	12.60
950523	130	8.71	272	11.45					
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950523	140	8.52	273	11.45	87.38 1013	0.86	253	36.75 -122.10	12.60
950523	150	8.49	270	11.50	86.42 1013	0.84	250	36.75 -122.11	12.60
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950523	210	8.91	259	11.36	87.09 1013				
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950523	220	8.86	273	11.29	87.32 1013	0.73	261	36.74 -122.12	12.70
950523	230	9.84	270	11.29	85.63 1013	0.66	259	36.74 -122.13	12.80
950523	240	9.99	261	11.31	85.43 1013	0.62	249	36.74 -122.13	12.70
950523	250	10.61	259	11.32	85.39 1013	0.63	244	36.74 -122.13	12.70
950523	300	10.37	264	11.32	85.52 1013.		249	36.74 -122.14	12.80
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950523	320	8.72	275	11.28	87.43 1014	0.80	254	36.74 -122.15	12.90
950523	330	8.38	281	11.28	87.96 1014	0.78	258	36.73 -122.15	13.00
950523					88.71 1014				
	340	8.02	281	11.33		0.87	257	36.73 -122.16	13.00
950523	350	7.13	279	11.33	89.92 1014	0.89	255	36.73 -122.16	13.10
950523	400	7.07	276	11.32	90.55 1014	0.92	255	36.73 -122.17	13.00
950523	410	7.93	256	11.30	89.76 1014	0.78	236	36.73 -122.18	12.90
950523	420	7.77	276	11.34	90.13 1014	0.85	252	36.73 -122.18	
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950523	430	7.59	279		90.32 1014	0.80		36.73 -122.19	13.00
950523	440	6.82	283	11.39	91.45 1014	0.92	256	36.73 -122.19	13.00
950523	450	6.47	282	11.27	92.03 1014	0.84	255	36.72 -122.20	12.90
950523	500	5.10	297	11.28	92.66 1014	0.88	266	36.72 -122.20	
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950523	510	4.66	295	11.31	93.19 1014	0.71	262	36.72 -122.21	13.00
950523	520	4.82	286	11.27	93.18 1014	0.52	248	36.72 -122.21	13.00
950523	530	4.51	279	11.33	93.58 1014	0.55	244	36.72 -122.22	13.00
950523	540	4.57	279	11.31	94.00 1014	0.64	252	36.72 -122.22	
									13.00
950523	550	4.41	285	11.29	94.31 1014	0.58	257	36.72 -122.22	13.10
950523	600	4.49	297	11.28	95.38 1014	0.82	261	36.72 -122.23	13.10
950523	610	4.26	291	11.31	95.86 1014	0.70	262	36.72 -122.23	13.20
950523	620	4.08	294	11.27	95.99 1014	0.73	266	36.72 -122.24	13.20
					96.19 1014	0.73			
950523	630	4.12	293	11.29			269	36.72 -122.24	13.30
950523	640	4.06	295	11.26	96.25 1014	0.65	267	36.72 -122.25	13.30
950523	650	3.62	295	11.31	96.53 1014	0.75	271	36.72 -122.25	13.30
950523	700	3.11	289	11.31	97.02 1014	0.69	272	36.72 -122.26	13.30
950523	710	3.40	290	11.33	97.36 1014	0.68	273	36.72 -122.26	13.40
950523	720	3.77	292	11.39	97.52 1013	0.65	279	36.72 -122.27	13.40

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36.72 -120.28
                                                                                       36.72 -122.27 13.40
950523
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0.83 255
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                                       11.40
                                                  97.77 1013
950523
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                                      11.44
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                                                                                        36.72 -122.28
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                                                 97.22 1013
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950523
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                                                97.09 1013
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950523
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                                                96.53 1013
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    36.71
    -122.30
    13.20

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    252
    36.71
    -122.31
    13.20

    0.59
    254
    36.71
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    13.20

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    13.20

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    13.20

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    13.10

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    13.10

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    13.10

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    36.70
    -122.33
    13.20

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    13.20

    0.83
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    13.20

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                      4.42
950523
            910
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                               310 11.83 92.24 1013
950523
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            920

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      11.82
      92.51
      1013

      4.91
      301
      11.77
      92.67
      1013

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      308
      11.70
      92.35
      1013

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4.76 78 36.78 -121.92
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36.81 -121.81
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36.81 -121.83 13.90
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14.10
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251
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92.13 1013
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94.04 1013
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92.07 1012
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36.77 -121.93 13.50
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0.61 258
0.63 255
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950524
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                                         90.61 1012
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36.77 -121.95 13.60
36.77 -121.95 13.50
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0.62 259

0.53 250

0.64 271

0.58 267

0.54 262
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91.17 1012
91.25 1012
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0.64 250
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0.61 263
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0.74 261
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0.79 265
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950524
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                                         91.99 1012
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36.76 -122.02
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91.64 1012
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				11.44	92.08 1012	0.76	289	36.76 -122.06	13.10
950524	440	6.90	300	11.44	92.18 1012	0.66	288	36.76 -122.06	13.20
950524	450	6.85	294	11.37	92.32 1012	0.63	289	36.77 -122.06	13.10
950524	500	6.83	290	11.32	92.05 1012	0.72	283	36.77 -122.07	
950524	510								13.10
		6.62	304	11.38	91.68 1012	1.37	111	36.77 -122.07	13.10
950524	520	5.82	303	11.41	92.03 1012	3.04	109	36.76 -122.05	13.20
950524	530	5.14	301	11.55	92.18 1012	3.05	110	36.76 -122.03	13.20
950524	540	5.41	293	11.51	91.74 1012	1.91	114	36.75 -122.02	
950524	550	5.67	289	11.38	91.59 1012			30.75 -122.02	12.90
						0.56	279	36.75 -122.01	12.90
950524	600	6.09	292	11.36	91.80 1012	0.51	288	36.75 -122.02	12.90
950524	610	6.02	291	11.35	91.50 1012	0.58	281	36.75 -122.02	12.80
950524	620	6.13	279	11.40	91.64 1012	0.52	271	36.75 -122.02	13.00
950524	630	6.03	279	11.39	91.25 1012	0.54	267		
950524	640	5.44	293					36.75 -122.03	13.00
				11.41	91.54 1012	0.60	278	36.75 -122.03	13.00
950524	650	5.39	290	11.36	90.87 1012	0.63	271	36.75 -122.04	13.00
950524	700	5.24	290	11.39	90.47 1012	0.64	276	36.75 -122.04	13.00
950524	710	4.75	305	11.44	90.70 1012	0.67	283	36.75 -122.04	12.90
950524	720	4.93	301	11.44	90.98 1012				
						0.66	286	36.75 -122.05	12.90
950524	730	4.38	307	11.45	90.63 1012	0.70	289	36.75 -122.05	13.10
950524	740	4.20	303	11.43	90.57 1012	0.69	291	36.76 -122.06	13.10
950524	750	4.54	318	11.43	90.76 1012	0.72	303	36.76 -122.06	13.20
950524	800	4.76	319	11.42	90.22 1012	0.60	326		
								36.76 -122.06	13.20
950524	810	4.67	328	11.48	90.15 1012	0.71	328	36.76 -122.07	13.20
950524	820	4.67	314	11.45	90.77 1012	0.66	322	36.77 -122.07	13.20
950524	830	5.09	327	11.43	90.69 1012	0.64	332	36.77 -122.07	13.20
950524	840	4.48	330	11.41	90.49 1012	0.72	334	36.77 -122.07	13.20
950524	850	4.53	315	11.47	90.69 1012	0.48	6	36.77 -122.08	
950524		4.53							13.20
	900		293	11.45	90.55 1012	2.85	114	36.77 -122.07	13.20
950524	910	4.71	296	11.42	90.63 1012	2.74	116	36.76 -122.05	13.10
950524	920	5.20	290	11.38	90.23 1012	2.78	124	36.76 -122.03	13.00
950524	930	5.28	283	11.38	89.96 1011	2.12	127	36.75 -122.02	13.00
950524	940	4.68	309	11.34	89.30 1011	0.76	315	36.75 -122.02	13.00
950524	950	4.82	302	11.35					
					90.01 1011	0.77	309	36.75 -122.02	12.90
950524		4.53	304	11.33	89.74 1011	0.79	307	36.75 -122.02	12.90
950524		4.47	296	11.30	90.07 1011	0.82	314	36.76 -122.03	12.80
950524	1020	4.99	306	11.34	89.88 1011	0.76	318	36.76 -122.03	12.90
950524	1030	4.21	315	11.31	89.18 1011	0.79	312	36.76 -122.04	12.90
950524	1040	4.49	301	11.33	89.37 1011	0.84	308	36.76 -122.04	12.90
950524		4.97	307	11.37	89.74 1011				
						0.84	315	36.77 -122.04	12.90
950524		4.43	309	11.28	89.53 1011	0.82	312	36.77 -122.05	12.90
950524		4.38	318	11.27	88.93 1011	0.78	315	36.77 -122.05	13.00
950524	1120	4.29	324	11.28	88.60 1011	0.75	324	36.78 -122.06	13.00
950524	1130	4.80	319	11.26	88.92 1011	0.62	329	36.78 -122.06	13.00
950524		4.09	297	11.27	89.02 1011	0.34	116	36.78 -122.06	
950524		5.95	290	11.16	88.63 1011				13.10
						2.69	128	36.77 -122.05	13.00
950524		4.85	287	11.16	88.23 1011	2.32	130	36.77 -122.04	12.90
950524		5.27	283	11.17	88.74 1011	2.23	130	36.76 -122.03	12.90
950524	1220	4.22	285	11.19	88.82 1011	1.90	134	36.75 -122.01	13.10
950524	1230	5.74	310	11.19	89.80 1011	0.65	320	36.75 -122.01	13.00
950524		6.22	309	11.12	88.37 1011				
						0.59	352	36.75 -122.01	13.00
950524		4.87	291	11.16	87.92 1011	4.56	73	36.76 -122.00	13.10
950524		4.93	276	11.14	88.38 1011	4.63	74	36.76 -121.97	13.40
950524	1310	5.20	272	11.16	88.67 1011	4.68	76	36.77 -121.94	13.40
950524	1320	4.93	265	11.12	88.63 1011	4.72	76	36.78 -121.91	13.30
950524		5.25	267	11.12	89.04 1011	4.68	75	36.78 -121.88	13.40
950524		4.83	257	11.10	89.62 1011				
						4.63	74	36.79 -121.85	13.60
950524		4.72	252	11.24	89.47 1011	4.74	71	36.80 -121.82	13.60
950524		4.82	253	11.17	90.23 1011	2.76	67	36.81 -121.79	13.30
950524		1.39	281	11.01	91.94 1011	0.46	196	36.80 -121.79	13.30
950524	1420	1.05	275	11.04	90.94 1011	0.00	242	36.80 -121.79	13.00

APPENDIX I. RADIOSONDE METEOROLOGICAL DATA

Sounding program REV 7.62 using Omega
Ship :PT_SUR
Location : 36.80 N 122.00 W 3 m
Rejected Sigma stations: a,b,c
Phase fitting length is 250 s from 0 min to 120 min

Sounding: 4
RS-number: 158735751 No PTU editing No wind editing

Started at: 16 MAY 95 14:59 GMT

Time	Asc	Rate Hgt/MS	SL Pres	sure Te	emp RH	D	ewp Di	r Spe	ed	WndStat
min	s	m/s	m	hPa	degC	%	degC	deg	m/s	·····ab ca c
		•			,		5 -	9	111, 0	
0	0	0.0	3	1013.8	11.4	94	10.5	36	2.5	
0	5	7.8	42	1009.0	11.7	75	7.5	111	////	CD-FGH-
0	10	5.7	60	1006.8	11.5	77	7.7	345		CD-FGH-
0	15	4.9	82	1004.1	11.6	72	6.8	111	////	
0	20	6.8	139	997.3	12.1	68	6.4	342		CD-FGH-
0	25	6.1	159	995.0	12.2	60	4.7	111	1111	
0	30	6.0	184	991.9	12.3	60	4.8	345		CD-FGH-
0	35	5.7	216	988.2	12.2	62	5.2	111	////	
0	40	6.3	248	984.5	12.1	61	4.9	345		CD-FGH-
0	45	6.6	276	981.1	11.9	62	4.9	111		CD-FGH-
0	50	5.7	309	977.3	11.7	63	4.9	344	3.1	CD-FGH-
0	55	6.0	336	974.1	11.6	64	5.1	111	////	CD-FGH-
1	0	6.0	364	970.9	11.6	64	5.1	342		CD-FGH-
1	5	5.7	390	967.8	11.7	63	4.9	///		CD-FGH-
1	10	6.0	427	963.5	11.6	63	4.9	343		CD-FGH-
1	15	6.2	455	960.2	12.0	60	4.5	111	////	CD-FGH-
1	20	5.7	480	957.4	12.4	58	4.4	342	3.3	CD-FGH-
1	25	5.7	510	953.9	12.4	57	4.2	///	////	CD-FGH-
1	30	5.9	541	950.4	12.1	58	4.1	343	3.5	CD-FGH-
1	35	6.1	572	946.9	11.8	58	3.9	///	. 1.111	CD-FGH-
1	40	5.8	600	943.7	11.5	59	3.8	343		CD-FGH-
. 1	45	5.7	626	940.8	11.3	60	3.9	///	////	CD-FGH-
1	50	5.7	651	938.0	11.0	61	3.8	343	4.0	
1	55	5.7	685	934.1	10.8	62	3.9	///		CD-FGH-
2	0	5.7	712	931.2	10.6	62	3.7	344	4.2	CD-FGH-
2	5	5.7	740	928.0	10.4	62	3.5	///	////	CD-FGH-
2	10	5.7	772	924.4	10.4	60	3.0	345	4.3	
2	15	5.9	804	920.9	10.4	59	2.8	///	////	CD-FGH-
2	20	6.0	831	917.8	10.1	59	2.5	346	4.4	CD-FGH-
2	25	6.1	863	914.4	9.9	59	2.3	///	////	
2	30	6.1	896	910.7	9.6	59	2.0	348		CD-FGH-
2	35	5.6	913	908.8	9.4	60	2.1	///		CD-FGH-
2	40	5.6	940	905.8	9.2	60	1.9	350		CD-FGH-
2	45	5.3	970	902.6	9.1	60	1.8	///	////	
2	50	5.3	991	900.3	8.9	60	1.6	352	4.3	CD-FGH-

Sounding program REV 7.62 using Omega
Ship :PT_SUR
Location: 36.80 N 121.80 W 3 m
Rejected Sigma stations: a,b,c
Phase fitting length is 250 s from 0 min to 120 min
Sounding: 5
RS-number: 309140543
No PTU editing

No PTU editing No wind editing

Started at: 16 MAY 95 18:01 GMT

Time min	AscRa s	ate Hgt/MSL m/s	Pres m	sure Te hPa	emp RH degC	\{\gamma}	Dewp Di degC	r Spe deg	ed m/s	WndStat
0	0	0.0	3	1013.4	12.1	90	10.5	279	2.2	
0	5	2.7	17	1011.7	13.3	70	8.0	///	1///	-BCDGH-
0	10	1.8	21	1011.3	13.0	72	8.1	285	2.3	-BCDGH-
0	15	1.7	31	1010.1	12.9	74	8.4	///	////	-BCDGH-
0	20	2.0	42	1008.8	12.8	75	8.5	281	2.1	-BCDGH-
0	25	1.7	46	1008.3	12.8	76	8.7	///	////	-BCD-FGH-
0	30	1.8	56	1007.1	12.6	77	8.7	281	2.3	-BCD-FGH-
0	35	1.8	70	1005.3	12.5	78	8.8	///	////	-BCD-FGH-
0	40	1.8	75	1004.9	12.5	78	8.8	261	2.3	-BCD-FGH-
0	45	1.8	83	1003.9	12.5	77	8.6	///		-BCD-FGH-
0	50	1.7	93	1002.6	12.5	75	8.2	257		-BCD-FGH-
0	55		103	1001.4	12.5	74	8.0	///	////	-BCD-FGH-
_ 1	0		113	1000.2	12.5	73	7.8	249		-BCD-FGH-
1	5		119	999.5	12.4	73	7.7	///		-BCD-FGH-
1	10		128	998.5	12.4	73	7.7	249		-BCD-FGH-
1	15		137	997.4	12.5	73	7.8	///		-BCD-FGH-
1	20		150	995.8	12.5	73	7.8	249		-BCD-FGH-
1	25		153	995.5	12.7	72	7.8	///		-BCD-FGH-
1	30		160	994.6	12.8	70	7.5	249		-BCD-FGH-
1	35		164	994.1	12.8	70	7.5	///		-BCD-FGH-
1	40		185	991.7	12.8	69	7.3	252		-BCD-FGH-
1	45		190	991.1	12.8	69	7.3	.///		-BCD-FGH-
1	50		201	989.8	12.8	69	7.3	250		-BCD-FGH-
1	55		208	988.9	12.7	69	7.2	///		-BCD-FGH-
2	0		218	987.8	12.6	69	7.1	247		-BCD-FGH-
2	5		228	986.6	12.6	69	7.1	///		-BCD-FGH-
2	10		234	985.9	12.5	69	7.0	247		-BCD-FGH-
2	15		244	984.7	12.4	69	6.9	///	////	-BCD-FGH-
2	20		256	983.3	12.3	68	6.6	247		-BCD-FGH-
2	25		266	982.1	12.3	69	6.8	///		-BCD-FGH-
2	30		275	981.1	12.1	69	6.6	253		-BCD-FGH-
2	35		283	980.1	12.1	69	6.6	///		-BCD-FGH
2	40		291	979.2	12.1	69	6.6	257		-BCD-FGH
2	45		302	977.9	11.9	70	6.7	///		-BCD-FGH
2	50		311	976.8	11.8	70	6.6	251		-BCD-FGH
2	55	1.8	320	975.7	11.9	71	6.9	///	////	-BCD-FGH

Start Up Date 16 MAY 95 20:09 GMT System test passed -No errors found Sounding program REV 7.62 using Omega

Ship :PT_SUR Location : 36.80 N 122.00 W

Rejected Sigma stations: a,b,c
Phase fitting length is 250 s from 0 min to 120 min

Sounding: 6

RS-number: 309140540

No PTU editing No wind editing

Started at: 16 MAY 95 20:17 GMT

Time min	AscRa s	ate Hgt/M m/s	SL Pres m	sure T hPa	emp RH degC	۲ او	Dewp Di degC	r Spe deg	ed m/s	WndStat
	s 0 5 10 15 20 25 30 35 40 45 50 5 10 5 10 5 10 5 10 5 10 5 10 5 10	m/s 0.0 -1.7 -1.0 -0.5 4.9 6.9 8.0 7.2 4.6 4.3 3.1 2.8 2.8 3.1 2.8 3.1 2.8 2.8						deg 292 ///	m/s 10.4 //// 10.5 //// 10.7 //// 9.9 //// 9.7 //// 9.1 //// 9.1 //// 9.1 //// 8.7 //// 8.8 ////	CD-FGHCD-FGHCD-FGHCD-FGHCD-FGHCD-FGHCD-FGHCD-FGHCD-FGHCD-FGHBCD-FGH-
2	30 35	2.9 2.8	551 565	947.4 945.8	14.0 14.0	37 37	-0.4 -0.4	299 ///		-BCD-FGH- -BCD-FGH-

Ship :PT_SUR Location : 36.80 N 121.80 W 3 m

Loran-C chain 1: 9940

Phase fitting length is 60 s from 0 min to 10 min Phase fitting length is 120 s from 10 min to 45 min Phase fitting length is 240 s from 45 min to 120 min

Sounding: 10 RS-number: 108234745

No PTU editing No wind editing

Started at: 17 MAY 95 17:47 GMT

Time	AscRa	ate Hgt/M:	SL Pres	sure Te	emp RH	De	ewp Di	r Spe	ed	WndStat
min	s	m/s	m	hPa	degC	%	degC	deg	m/s	
0	0	0.0	3	1016.8	12.4	88	10.5	278	1.0	000000000
0	5	4.2	. 24	1014.1	12.7	63	5.9	///	////	111100000
0	10	4.1	44	1011.7	12.4	66	6.3	268	2.2	111100000
0	15	3.8	60	1009.8	12.3	69	6.8	///	////	111100000
0	20	3.5	74	1008.0	12.1	70	6.8	263	2.5	111100000
0	25	3.5	91	1006.1	12.0	72	7.2	///	////	111100000
0	30	3.5	107	1004.1	11.8	72	7.0	263	2.3	111100000
0	35	3.4	125	1001.9	11.6	73 ·	7.0	111		111100000
0	40	3.3	144	999.7	11.4	74	7.0	259	2.4	111100000
0	45	3.3	158	998.0	11.3	75	7.1	///		111100000
0	50	3.3	174	996.1	11.1	76	7.1	256		111100000
0	55	3.7	198	993.1	10.9	77	7.1	///		111100000
1	0	3.5	213	991.5	10.7	78	7.1	254		111100000
1	5	3.6	234	988.9	10.5	79	7.1	///		111100000
1	10	3.7	255	986.4	10.3	80	7.1	250		111100000
1	15	4.0	280	983.5	10.0	82	7.1	///		111100000
1	20	4.3	302	980.9	9.8	83	7.1	251		111100000
1	25	3.9	318	978.9	9.7	85	7.3	///-		111100000
1	30	4.0	332	977.3	9.5	85	7.2	250		111100000
1	35	3.8	346	975.6	9.4	86	7.2	///		111100000
1	40	4.0	375	972.3	9.1	88	7.3	246		111100000
1	45	4.0	399	969.4	8.9	89	7.2	///		111100000
1	50	3.8	417	967.3	8.6	89	6.9	247		111100000
1	55	4.0	434	965.3	8.6	90	7.1	///		111100000
2	0	4.2	457	962.6	8.4	90	6.9	241		111100000
2	5	4.6	483	959.5	8.2	90	6.7	///		111100000
2	10	4.5	509	956.5	8.1	91	6.8	237		111100000
2	15	4.6	537	953.4	8.1	88	6.3	///		111100000
2	20	4.4	548	952.1	8.7	79	5.3	240		111100000
2	25	4.2	562	950.4	10.2	70	5.0	///		111100000
2	30	4.0	576	948.8	11.8	63	5.0	240		111100000
2	35	3.4	590	947.2	12.6	59	4.9	///		111100000
2	40	3.2	605	945.6	12.7	55	4.0	237		111100000
2	45	2.8	620	943.9	12.8	52	3.3	///		111100000
2	50	2.9	635	942.1	13.1	50	3.0	236	4.2	111100000

Ship :PT_SUR Location : 36.80 N 122.00 W

Loran-C chain 1: 9940

Phase fitting length is 60 s from 0 min to 10 min
Phase fitting length is 120 s from 10 min to 45 min
Phase fitting length is 240 s from 45 min to 120 min

Sounding: 11 RS-number: 108234743

No PTU editing No wind editing

Started at: 17 MAY 95 21:54 GMT

Time min	Asc s	Rate Hgt/MS m/s	SL Pres m	sure Te	emp RH degC	De %		r Spe deg		WndStat
	\$ 05105205305405505105205	m/s 0.0 3.8 4.1 4.2 4.1 3.8 3.7 3.5 3.2 3.3 3.3 3.3 3.4 3.5 3.3 3.4	m 3 20 44 67 85 100 115 129 148 160 185 197 215 229 250 265 284 296	hPa 1016.3 1014.1 1011.3 1008.4 1006.3 1004.5 1002.6 1000.9 998.7 997.3 994.4 992.9 990.7 989.0 986.6 984.8 982.5 981.1	degC 12.2 13.3 12.6 12.4 12.2 12.1 11.9 11.8 11.6 11.5 11.3 11.2 11.0 10.9 10.7 10.7 10.5 10.4	% 96 72 76 78 79 81 83 84 85 86 87 86 87 87	degC 11.6 8.4 8.5 8.7 9.0 9.2 9.1 9.0 8.9 8.9 9.0 8.7 8.7 8.7 8.5 8.4	deg 261 /// 309 /// 302 /// 300 /// 286 /// 272 /// 281 /// 291 ///	m/s 5.4 //// 5.3 //// 5.7 //// 5.8 //// 7.0 //// 9.7 //// 8.0 //// 7.1 //// 7.3 ////	000000000 111100000 111100000 111100000 111100000 111100000 111100000 111100000 110100000 111100000 111100000 111100000 111100000 111100000 111100000 111100000
1 1 1 1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	30 35 40 45 50 55 0 51 10 12 25 30 34 45 45	3.2 3.4 3.4 3.4 3.4 3.4 3.7 3.4 3.7 3.4 3.3 3.4 3.4 3.4 3.4 3.5 3.4 3.4 3.4 3.7 3.7 3.7 3.7 3.7 3.7 3.7 3.7 3.7 3.7	312 336 351 368 379 401 416 439 452 468 490 505 522 538 555 571	979.2 976.4 974.7 972.6 971.3 968.7 967.1 964.4 962.8 960.9 958.4 956.6 954.6 952.9 950.9 949.1	10.2 10.1 9.9 9.7 9.6 9.6 9.4 9.3 9.2 9.1 8.9 9.4 9.5 9.8	87 88 88 89 90 91 91 92 91 91 89 88 83 78	8.2 8.2 8.1 8.0 7.9 8.1 7.9 8.0 7.9 7.6 7.6 7.7 7.1 6.6	291 /// 292 /// 290 /// 288 /// 287 /// 285 /// 283 ///	7.2 //// 7.1 //// 7.2 //// 7.0 //// 6.9 //// 6.5 ////	111100000 111100000 111100000 111100000 111100000 111100000 111100000 111100000 111100000 111100000 111100000 111100000 111100000

Ship :PT_SUR Location : 36.70 N 121.90 W

Loran-C chain 1: 9940

Phase fitting length is 60 s from 0 min to 10 min Phase fitting length is 120 s from 10 min to 45 min Phase fitting length is 240 s from 45 min to 120 min

Sounding: 14 RS-number: 108234746

No PTU editing No wind editing

Started at: 18 MAY 95 15:17 GMT

Time	AscRat	e Hgt/MSL	Pres	sure Te	mp RH	De	wp Di:	r Spe	ed	WndStat
min	s	m/s	m	hPa	degC	용	degC	deg	m/s	
							,	,		
0	0	0.0	3	1016.6	10.4	93	9.3	237	0.6	000000000
0	5	4.0	25	1014.0	11.6	72	6.8	111	1111	111100000
0	10	3.5	38	1012.5	11.0	75	6.8	240		111100000
0	15	3.8	57	1010.1	10.9	78	7.3	111		111100000
0	20	3.5	72	1008.3	10.8	79	7.4	241		111100000
0	25	3.3	85	1006.7	10.7	81	7.6	///		111100000
0	30	3.3	103	1004.6	10.5	82	7.6	237		111100000
0	35	3.3	123	1002.2	10.3	83	7.6	111	////	111100000
0	40	3.5	143	999.7	10.1	84	7.6	254.	0.5	111100000
0	45	3.5	163	997.3	10.0	85	7.6	///	////	111100000
0	50	3.7	182	995.1	9.7	86	7.5	243		111100000
0	55	3.8	198	993.1	9.6	88	7.8	///		110100000
1	0	3.7	214	991.2	9.4	88	7.6	246		110100000
1	5	3.7	234	988.8	9.3	89	7.6	///	////	
1	10	3.8	256	986.1	9.1	90	7.6	254		111100000
1	15	3.6	274	984.0	8.9	91	7.6	///	////	
. 1	20	3.6	291	982.1	8.8	92	7.6	274		111100000
1	25	3.6	304	980.5	8.7	92	7.5	///	////	
1 1	30 35	3.6	321	978.5	8.6	92	7.4	313		111100000
1	40	3.6	341 367	976.1	8.5	93	7.5	///	////	
. 1	45	3.7 3.8	385	973.0 970.9	8.4	93	7.4	326		111100000
1	50	3.8	405	968.5	8.3 8.1	93 93	7.3	///	////	
1	55	3.9	423	966.4	8.1	93 94	7.1 7.2	334		111100000
2	0		437	964.7	8.0	94	7.1	/// 347	////	
2	5	3.7	454 .		7.9	94	7.1	///		111100000
. 2	10	3.5	472	960.7	7.8	94	6.9	338	////	111100000 111100000
2	15		493	958.3	7.7	94	6.8	///		111100000
2	20		510	956.3	7.6	94	6.7	336		111100000
2	25		528	954.2	7.5	94	6.6	///		111100000
2	30		548	951.8	7.4	94	6.5	338		111100000
2	35	3.9	567	949.6	7.3	94	6.4	///		111100000
2	40	3.7	582	947.9	7.2	94	6.3	348		111100000
2	45	3.7	604	945.4	7.0	94	6.1	///		111100000

Sounding program REV 7.62 using Omega Ship :PT_SUR Location : 36.80 N 121.90 W 3 m

Rejected Sigma stations: a,b,c
Phase fitting length is 250 s from 0 min to 120 min
Sounding: 16
RS-number: 158735752

No PTU editing No wind editing

Started at: 18 MAY 95 21:53 GMT

Time min	Asc s	Rate Hgt/MSL m/s	Pres m	ssure Te hPa	mp RH degC	D %	ewp Di: degC	r Spe deg	ed m/s	WndStat
	0 5 10 15	m/s 0.7 4.5 5.2 5.5 5.5 5.1 4.0 9 7 3.7 7 3.6 3.1 3.3 3.6 3.6 3.7						deg 255 /// 287 /// 288 /// 277 /// 277 /// 264 /// 258 /// 260 /// 261 /// 261 ///	m/s 6.3 //// 4.3 //// 3.9 //// 3.5 //// 2.8 //// 2.3 //// 2.3 //// 2.3 //// 2.3 //// 2.3 //// 2.1 //// 2.0 ////	CDGHCDGHCDGHCDGHCDGHCDGHCDGHCDFGH
2 2 2	45 50 55	3.3 3.5	693 711 730	935.0 933.0 930.9	16.3 16.2 16.1	38 39 41	2.0 2.3 2.9	266 /// 267 ///		

Sounding program REV 7.62 using Omega Ship :PT_SUR

Location: 36.78 N 121.90 W

Rejected Sigma stations: a,b,c
Phase fitting length is 250 s from 0 min to 120 min
Sounding: 18
RS-number: 158735842

No PTU editing No wind editing

Started at: 19 MAY 95 15:35 GMT

Time	AscRate	e Hgt/MS	L Press	sure Te	mp RH	De	wp Di:	r Spe	ed	WndStat
min	s	m/s	m	hPa	degC	왕	degC	deg	m/s	
•	•		_							
0	0	0.0	3	1014.6		100	10.0	93	0.9	
0	5	3.3	22	1012.4	11.0	80	7.7	///		CD-FGH
0	10	3.9	42	1010.0	10.7	81	7.6	. 9	1.4	
0	15	3.4	55	1008.4	10.7	83	8.0	///	////	
0	20	3.3	70	1006.6	10.5	84	8.0	6		CD-FGH
0	25	3.3	87	1004.5	10.4	86	8.2	///		CD-FGH
0	30	3.3	102	1002.6	10.3	86	8.1	1		CD-FGH
0	35	3.4	122	1000.3	10.2	87	8.2	///	////	
0	40	3.3	141	998.0	10.1	87	8.1	5		CD-FGH
0	45	3.4	156	996.2	10.0	88	8.1	///		CD-FGH
0	50	3.4	173	994.1	9.9	88	8.1	15		CD-FGH
0	55	3.4	189	992.2	9.8	88	8.0	///	////	
1	0	3.4	204	990.5	9.7	88	7.9	23		CD-FGH
1	5	3.3	220	988.6	9.7	89	8.0	///		-BCD-FGH
1	10	3.2	238	986.4	9.6	89	7.9	23		-BCD-FGH
1	15	3.3	255	984.3	9.5	89	7.8	///		-BCD-FGH
1	20	3.2	270	982.5	9.4	89	7.7	24		-BCD-FGH
1	25	3.3	289	980.3	9.3	89	7.6	///		-BCD-FGH
	-30	3.4	305	978.5	9.2	89	7.5	29		-BCD-FGH
1	35	3.4	322	976.4	9.1	89	7.4	///	////	
. 1	40	3.4	341	974.2	9.0	89	7.3	33		-BCD-FGH
1	45	3.3	354	972.6	9.0	89	7.3	///		-BCD-FGH
1	50	3.3	369	970.9	9.2	89	7.5	31		-BCD-FGH
1	55	3.2	382	969.3	10.1	90	8.6	///		-BCD-FGH
2	0	3.0	395	967.8	10.6	90	9.1	30		-BCD-FGH
2	5	2.9	409	966.2	11.4	90	9.9	///		-BCD-FGH
2	10	2.6	418	965.2	11.6	88	9.7	28	2.3	
2	15	2.5	429	963.9	12.1	88	10.2	///	////	
2	20	2.3	438	962.8	12.3	86	10.1	31		-BCD-FGH
2	25	2.5	454	960.9	12.3	82	9.4	///		-BCD-FGH
2	30	2.4	467	959.5	12.4	78	8.7	31		-BCD-FGH
2	35	2.4	481	957.9	12.5	78	8.8	///		-BCD-FGH
2	40	2.5	493	956.5	12.9	79	9.4	38		-BCD-FGH
2	45	2.6	506	955.0	13.2	80	9.9	///		-BCD-FGH
2	50	2.7	518	953.7	13.3	81	10.2	44		-BCD-FGH
2	55	2.6	533	952.0	13.7	77	9.8	///	////	-BCD-FGH

Ship :PT_SUR Location : 36.80 N 121.80 W

Loran-C chain 1: 9940

Phase fitting length is 60 s from 0 min to 10 min Phase fitting length is 120 s from 10 min to 45 min Phase fitting length is 240 s from 45 min to 120 min

Sounding: 19

RS-number: 108234748

No PTU editing No wind editing

Started at: 19 MAY 95 18:27 GMT

Time min	Aso	cRate Hgt/MSL m/s	Pres	sure hPa	Temp	RH ~C	Dew		Spe		WndStat
шти	3	III/ S	111	11120	a de	yC	용 (degC	deg	m/s	
0	0	0.0	3	1013.4	4 10	.5 9	6	9.9	263	1 /	000000000
Õ	5	2.7	13	1012.2					///		110100000
0	10	2.6	29	1010.					299		110100000
0	15	3.2	51	1007.					///	1111	
0	20	3.5	72	1005.					281		111100000
0	25	3.7	95	1002.					///		111100000
0	30	3.7	115	1000.0	0 10				271		111100000
0	35	3.9	136	997.	4 10	.3 9	0 .		///	1111	
0	40		147	996.			0	8.8	318	1.3	111100000
0	45		161	994.		.3 9	0	8.8	///	////	111100000
0	50		179	992.2					250		111100000
0	55		200	989.8					///		111100000
1	0		216	. 987.8					270		111100000
1	5		234	985.		.9 9			///		111100000
1	10		244	984.		.8 9		8.3	12		111100000
1	15		257	982.		.8 9			///		111100000
1	20		281	980.		.7 8		8.0	14		111100000
1	25		300	977.		.7 8			///		111100000
1	30		305	977.3		.6 8			358		111100000
1	35		337	973.		.5 8			///		111100000
1	40		353	971.0		.4 8		7.7	0		111100000
1 1	45		369	969.8		.3 8			///	////	111100000
1	50 55		386	967.8		.1 8		7.3	4		111100000
2	0		398 406	966.4 965.4					///	////	111100000
2	5		419	963.				9.9 10.4	31 ///	1.0	111100000 111100000
2	10		443	961.				9.4	44		111100000
2	15		449	960.					///	////	111100000
2	20		449	960.				8.3	52	1.5	111100000
. 2	25		490	955.					///	////	111100000
2	30		498	954.				8.4	66		111100000
2	35		515	952.	9 14				///	1111	111100000
2	40		527	951.					107	1.2	111100000
2	45		544	949.					///	////	111100000

Sounding program REV 7.62 using Loran-C :PT SUR Location : 36.80 N 122.00 W Loran-C chain 1: 9940 Phase fitting length is 60 s from 0 min to 10 min Phase fitting length is 120 s from 10 min to 45 min Phase fitting length is 240 s from 45 min to 120 min Sounding: 20 RS-number: 108234840 No PTU editing No wind editing Sounding program REV 7.62 using Loran-C :PT SUR Location: 36.80 N 122.00 W Loran-C chain 1: 9940 Phase fitting length is 60 s from 0 min to 10 min Phase fitting length is 120 s from 10 min to 45 min Phase fitting length is 240 s from 45 min to 120 min Sounding: 20 RS-number: 108234753 No PTU editing No wind editing Started at: 19 MAY 95 21:31 GMT

T: WndSt		AscRate	Hgt/MSL	Pressure	Temp	RH	Dewp	Dir	Speed	
min	s	m/s	m	hPa	degC	양	degC	deg	m/s	
0	0	0.0	3	1012.3	11.0	95	10.2	275	6.1	000000000
0	5	1.3	9	1011.5	12.4	71	7.3	111	1111	111100000
0	10	2.7	30	1009.0	11.8	74	7.4	292	5.8	111100000
0	15	3.3	53	1006.2	11.6	75	7.4	111	////	111100000
0	20	3.5	72	1003.9	11.4	76	7.4	289	6.3	111100000
0	25	3.3	84	1002.4	11.2	78	7.6	111	1111	111100000
0	30	3.3	103	1000.2	11.0	79	7.5	294	5.7	111100000
0	35	3.9	125	997.5	10.8	81	7.7	111	1111	111100000
0	40	3.8	143	995.3	10.6	81	7.5	293	5.7	111100000
0	45	3.5	157	993.6	10.5	81	7.4	111	1111	111100000
0	50	3.3	170	992.2	10.4	82	7.5	296		111100000
0	55	3.2	182	990.7	10.3	83	7.6	///	1111	111100000
1	0.	3.0	192	989.5	10.3	82	7.4	298	4.8	111100000
1	5	2.6	204	988.1	10.2	82	7.3	111	1111	111100000
1	10	2.4	216	986.6	10.3	81	7.2	298	4.4	111100000
1	15	2.3	229	985.1	10.4	79	7.0	///	////	111100000
1	20	2.4	241	983.7	10.9	79	7.5	292	4.2	111100000
1	25	2.3	251	982.5	11.2	79	7.7	111	////	111100000
1	30	2.2	259	981.6	11.4	79	7.9	292	3.8	111100000
1	35	2.3	274	979.8	11.5	79	8.0	111	////	111100000
1	40	2.3	285	978.5	11.5	79	8.0	285	3.7	111100000
1	45	2.3	298	977.0	11.6	79	8.1	///	////	111100000
1	50	2.2	308	975.8	12.0	77	8.1	279	3.5	111100000
1	55	2.2	318	974.7	13.2	59	5.4	///	1111	111100000
2	0	2.3	328	973.5	14.6	43	2.2	276	3.4	111100000
2	5	2.3	340	972.0	15.5	43	3.0	///	////	111100000
2	10	2.1	349	971.1	15.9	57	7.5	273	3.2	111100000
2	15	2.2	363	969.4	16.0	57	7.6	111	1///	111100000
2	20	2.2	374	968.2	16.4	52	6.6	275	2.8	111100000

2 2 3 3 5 0 5 0 5 0 5 0 5 0 5 0 5 0 5 0 5 0	2.2 2.3 2.2 2.3 2.2 2.2 2.1 2.0 1.9 1.9 1.8 1.8 1.7 1.7 1.7 1.7 1.5 1.5 1.5 1.5 1.5 1.5 1.3 1.3 1.3	385 396 407 428 440 450 478 488 498 517 5234 498 517 5234 5511 5510 5610 6610 6610 6610 6610 6610	966.9 965.7 964.5 963.3 962.1 969.5 95	16.9 17.7 18.1 18.0 17.9 17.9 18.1 18.4 18.4 18.4 18.5 18.4 18.5 18.7 19.1 19.2 19.1 19.2 19.1 19.1 19.2 19.1 19.3 19.3 19.3	54474899987665544211218777666555556518439	7.3 7.7 6.7 7.1 7.1 7.0 6.6 6.3 4.0 4.2 3.8 6.5 4.2 4.1 8.8 7.2 4.1 8.8 7.3 7.3 7.3 7.3 7.3 7.3 7.3 7.4 7.5 7.5 7.6 7.7 7.7 7.7 7.7 7.7 7.7 7.7	/// 277 /// 282 /// 284 /// 285 /// 306 /// 301 /// 283 /// 285 /// 288 /// 271 /// 265 /// 259 /// 250 /// 250 ///	2.4 //// 2.0 //// 1.7 /// 1.6 //// 1.3 //// 1.2 //// 1.1 //// 1.1 //// 1.5 //// 1.8 //// 2.0 //// 3.9 //// 3.9 //// 4.0	111100000 111100000
5 20 5 25 5 30	1.3 1.3 1.3	686 694 699	933.4 932.6	19.2 19.3	28 24	0.3 -1.7	253 ///	3.9 ////	111100000 111100000 111100000 111100000 111100000 111100000

Ship :PT SUR

Location : $3\overline{6}.80 \text{ N } 122.00 \text{ W}$ 3 m

Loran-C chain 1: 9940

Phase fitting length is 60 s from 0 min to 10 min Phase fitting length is 120 s from 10 min to 45 min Phase fitting length is 240 s from 45 min to 120 min

Sounding: 21

RS-number: 108234651

No PTU editing No wind editing

Started at: 19 MAY 95 21:55 GMT

	AscRate	Hgt/MSL	Pressure	Temp	RH	Dewp	Dir	Speed	
min s	m/s	m	hPa	degC	ક	degC	deg	m/s	
WndStat min s 0 0 0 5 0 10 0 15 0 20 0 25 0 30 0 35 0 40 0 45 0 50 1 5 1 10 1 15 1 20 1 25 1 30 1 35 1 40 1 45 1 50 1 55 2 0 2 5 2 10		m 3 20 38 60 74 93 109 125 141 157 172 191 218 239 263 278 295 311 332 348 364 379 395 412 431 445 458	hPa 1013.9 1011.9 1009.8 1007.1 1005.3 1003.1 1001.2 9997.3 995.3 995.3 995.3 995.3 995.4 963.3 965.4 963.3 961.7	degC 11.0 12.0 11.7 11.5 11.3 11.1 11.0 10.8 10.6 10.5 10.4 10.0 10.3 10.6 11.1 11.3 11.4 11.9 13.8 15.0 15.6 16.3 17.3 17.9 17.9	% 95174677901123555420912004113779049	degC 10.2 7.3 7.5 7.7 7.6 7.7 7.6 7.7 7.6 7.6 7.7 7.6 7.6	deg 276 /// 304 /// 308 /// 312 /// 315 /// 308 /// 294 /// 287 /// 286 /// 279 /// 274	m/s 5.8 //// 6.5 //// 5.9 //// 5.1 //// 4.6 //// 4.1 //// 3.7 //// 3.5 //// 2.7 //// 2.5	111100000 111100000
2 15 2 20 2 25 2 30 2 35 2 40 2 45	3.2 3.2 3.2 2.9 2.9	474 491 508 526 535 545 569	958.4 956.5 954.5 952.5 951.6 950.4 947.8	17.9 17.8 17.9 18.1 18.4 18.7	49 50 49 47 45 42	7.1 7.3 7.1 6.7 6.3 5.6 5.3	/// 273 /// 272 /// 273 ///	////	111100000 111100000 111100000 111100000

:PT SUR Ship

Location: 36.70 N 122.40 W

Loran-C chain 1: 9940

Phase fitting length is 60 s from 0 min to 10 min Phase fitting length is 120 s from 10 min to 45 min Phase fitting length is 240 s from 45 min to 120 min

Sounding: 23 RS-number: 108234843

No PTU editing No wind editing

Started at: 20 MAY 95 15:19 GMT

Ti WndSt		AscRate	Hgt/MSL	Pressure	Temp	RH	Dewp	Dir	Speed	
min	S	m/s	m	hPa	degC	90	degC	deg	m/s	
0	0	0.0	3	1014.9	11.1	87	9.0	326	4.2	000000000
0	5	6.5	. 31	1011.5	12.1	65	5.8	111	1111	111100000
0	10	5.5	58	1008.3	11.6	67	5.7	326	3.7	111100000
	15	6.0	93	1004.1	11.3	71	6.3	111	////	111100000
0	20	6.0	123	1000.4	10.9	72	6.1	329	3.5	111100000
	25	6.1	156	996.4	10.7	74	6.3	111	////	111100000
	30	6.1	186	992.9	10.3	75	6.1	325	3.5	111100000
	35	5.9	214	989.5	10.1	77	6.3	///	////	111100000
	40	6.3	247	985.7	9.7	78	6.1	320	3.5	111100000
	45	5.9	269	983.0	9.5	79	6.1	///	////	111100000
	50	6.1	305	978.7	9.2	80	6.0	311	3.5	111100000
	55	5.9	331	975.6	8.9	82	6.0	///	////	111100000
1	0	5.7	356	972.7	8.7	83	6.0	316	3.3	111100000
1	5	5.9	391	968.6	8.4	85	6.1	///	////	111100000
	10	5.8	420	965.2	8.0	86	5.8	323	3.2	111100000
	15	6.0	452	961.4	7.8	88	6.0	///	////	111100000
	20	5.8	480	958.1	7.6	89	5.9	330	3.0	111100000
	25	5.9	513	954.3	7.4	89	5.8	///	////	111100000
1	30	6.3	544	950.7	7.2	89	5.6	324	2.6	111100000
	35	6.2	572	947.4	7.0	90	5.5	///	////	111100000
	40	6.4	613	942.8	6.8	90	5.3	344	2.4	111100000
	45 50	5.9 5.8	629	941.0	6.7	90	5.2	///	////	111100000
1	55	6.1	655 692	938.0	6.4	90	4.9	309	1.6	111100000
2	0	6.5	738	933.7 928.4	6.1	90	4.6	///	////	111100000
2	5	6.0	760	925.9	6.0	27	-11.5	265	1.9	111100000
	10	5.7	783	923.9	7.2 10.2	19 14	-14.9	///	////	111100000
	15	5.7	801	923.3	13.2	10	-16.1	241	1.8	111100000
	20	5.5	821	919.2	15.3	9	-17.7 -17.4	/// 237	//// 1.9	111100000 111100000
	25	4.5	830	918.3	15.9	11	-17.4 -14.5	///	////	111100000
	30	3.7	848	916.3	16.1	11	-14.3	230	2.1	111100000
	35	3.6	865	914.5	16.0	11	-14.4	///	////	111100000
	40	3.3	883	912.5	16.0	10	-15.6	226	2.3	111100000
	45	3.3	902	910.5	16.0	8	-18.2	///	////	111100000
				· -		-		, , ,	,,,,	

Sounding program REV 7.62 using Loran-C Ship :PT SUR Location : $3\overline{6}.70 \text{ N } 122.40 \text{ W}$ Loran-C chain 1: 9940 Phase fitting length is 60 s from 0 min to 10 min Phase fitting length is 120 s from 10 min to 45 min Phase fitting length is 240 s from 45 min to 120 min Sounding: 24 RS-number: 108234747 No PTU editing No wind editing Sounding program REV 7.62 using Loran-C :PT SUR Location: 36.70 N 122.40 W 3 m Loran-C chain 1: 9940 Phase fitting length is 60 s from 0 min to 10 min Phase fitting length is 120 s from 10 min to 45 min Phase fitting length is 240 s from 45 min to 120 minSounding: 24 RS-number: 108234747

No PTU editing No wind editing

Started manually by operator

Started at: 20 MAY 95 17:26 GMT

T: WndSt		AscRate	Hgt/MSL	Pressure	Temp	RH	Dewp	Dir	Speed	
min	s	m/s	m	hPa ·	degC	90	degC	deg	m/s	
0 0 0	0 5 10	0.0 175.5 104.2	3 1057 1045	1015.2 895.4 896.6	11.2 15.6 15.8	84 11 11	8.6 -14.7 -14.6	355 /// ///	2.3 ////	00000000 000100000 000100000
0	15 20	64.7	1041 1021	897.0 899.2	15.9 16.0	11 10	-14.5 -15.6	/// 204	//// 5.6	011100000 011100000
0 0	25 30	39.0 33.4	1017 1006	899.5 900.7	16.0 16.0	10 10	-15.6 -15.6	/// 211	//// 3.2	111100000 111100000
0	35 40	-2.1 -1.8	997 990	901.7 902.5	16.0 15.9	11 11	-14.4 -14.5	/// 225		111100000
0 0 0	45 50 55	-2.1 -1.7 -2.0	979 969 960	903.6 904.7 905.7	15.9 16.0 16.1	11 12 11	-14.5 -13.3 -14.3	/// 232 ///	//// 4.1 ////	111100000 111100000 111100000
1 1	0 5	-1.9 -1.8	950 941	906.7 907.7	16.1 16.2	11 11	-14.3 -14.3	222		111100000
1 1	10 15	-2.0 -1.9	930 921	908.9 909.8	16.3 16.3	11 11	-14.2 -14.2	231	2.8	111100000 111100000
1	20 25	-1.9 -1.9	913 902	911.9	16.3 16.4	12 13	-13.1 -12.0	231	2.0	111100000 111100000
1 1 1	30 35 40	-1.9 -2.0 -1.8	892 882 876	912.9 914.0 914.7	16.4 16.5 16.5	12 12 12	-13.0 -12.9 -12.9	232 /// 234	2.5 //// 3.0	111100000 111100000 111100000
1 1 1	45 50 55	-1.8 -1.9 -2.0	865 855 844	915.8 916.9 918.2	16.5 16.5 16.5	12 12 12	-12.9 -12.9 -12.9	/// 235 ///	3.0 //// 3.2 ////	111100000 111100000 111100000

:PT SUR

Location: 36.70 N 122.40 W

Loran-C chain 1: 9940

Phase fitting length is 60~s from 0~min to 10~min Phase fitting length is 120~s from 10~min to 45~minPhase fitting length is 240 s from 45 min to 120 min

Sounding: 25

RS-number: 108234749

No PTU editing No wind editing

Ground check : Corr Ref RS Pressure : 1016.2 1016.2 -0.0 Temperature: 22.7 22.7 0.0 Humidity : 42 42 0

Started manually by operator Started at: 20 MAY 95 17:52 GMT

Time WndStat		Hgt/MSL	Pressure	Temp	RH	Dewp	Dir	Speed	
min s		m	hPa	degC	엉	degC	deg	m/s	
0 0	0.0	3	1016.2	11.2	88	9.3	25	1.9	000000000
0 5	0.0	2	1016.3	12.9	73	8.2	111	1111	111100000
0 10	-0.2	1	1016.5	12.9	72	8.0	219	2.2	111100000
0 15	-0.1	1	1016.5	12.9	72	8.0	111	////	
0 20	-0.1	1	1016.5	12.8	73	8.1	228	2.8	111100000
0 25	-0.2	1	1016.5	12.8	73	8.1	///	////	
0 30	-0.1	1	1016.5	12.7	73	8.0	234	2.7	111100000
0 35	-0.1	1	1016.5	12.7	74	8.2	111	////	111100000
0 40		1	1016.5	12.6	74	8.1	242	2.4	111100000
0 45		1	1016.5	12.6	74	8.1	///	////	111100000
0 50		1	1016.5	12.6	74	8.1	287	0.8	111100000
0 55		1	1016.5	12.6	74	8.1	111	////	111100000
1 0		1	1016.5	12.5	74	8.0	324	1.0	111100000
1 5		-2	1016.8	12.5	75	8.2	///	////	
1 10		-1	1016.7	12.5	75	8.2	325		111100000
1 15		-2	1016.8	12.4	74	7.9	///	////	
1 20		-1	1016.7	12.4	. 77	8.5	323	1.9	
1 25		-1	1016.7	12.3	77	8.4	///	1///	
1 30		-1	1016.7	12.3	77	8.4	311		111100000
1 35		-3	1016.9	12.5	78	8.8	///	////	111100000
1 40		3	1016.2	12.2	77	8.3	316	2.5	111100000
1 45		8	1015.6	12.4	77	8.5	///	////	
1 50		9	1015.5	12.3	76	8.2	318	2.7	111100000
1 55		8	1015.6	12.4	76	8.3	///	////	
2 0		9	1015.5	12.6	76	8.5	318	2.7	111100000
2 5		9	1015.5	12.4	75	8.1	///	////	
2 10		7	1015.7	12.5	75	8.2	314	2.9	
2 15		10	1015.3	12.5	76	8.4	///	////	
2 20		7	1015.7	12.4	75	8.1	313	3.2	111100000
2 25		7	1015.7	12.6	76	8.5	///	////	
2 30		7	1015.7	12.6	76	8.5	311	3.2	111100000
2 35		5	1016.0	12.7	75	8.4	///	////	
2 40		1	1016.5	12.6	75	8.3	312	3.1	111100000
2 45		0	1016.6	12.6	75	8.3	///	////	
2 50	-0.3	-1	1016.7	12.9	75	8.6	317	3.1	111100000

Sounding program REV 7.62 using Loran-C Ship :PT_SUR Location : 36.70 N 122.40 W 3 m

Loran-C chain 1: 9940

Phase fitting length is 60 s from 0 min to 10 min Phase fitting length is 120 s from 10 min to 45 min Phase fitting length is 240 s from 45 min to 120 min

Sounding: 25

RS-number: 108234749

No PTU editing No wind editing

Ground check : Ref RS Corr Pressure : 1016.9 1016.9 0.0 Temperature : 13.3 13.3 -0.0 Humidity : 71 71 0

Started manually by operator

Started at: 20 MAY 95 19:54 GMT

T: WndSt		AscRate	Hgt/MSL	Pressure	Temp	RH	Dewp	Dir	Speed	
min	s	m/s	m	hPa	degC	90	degC	deg	m/s	•
0	0	0.0	3	1016.9	13.3	71	8.2	124		000000000
0	5	0.0	3	1016.9	13.2	72	8.3	///	////	111100000
0	10	0.4	7	1016.5	13.1	72	8.2	218	1.2	111100000
0	15	0.0	3	1016.9	13.2	72	8.3	///	////	111100000
. 0	20	0.0	3	1016.9	13.0	71	7.9	217	1.2	111100000
0	25	0.0	4	1016.8	13.0	72	8.1	///	////	111100000
0	30	0.0	3	1016.9	12.7	70	7.4	218	1.1	111100000
0	35	0.0	2	1017.1	13.0	71	7.9	///	////	111100000
0	40	-0.1	3	1016.9	13.1	71	8.0	216	0.8	111100000
0	45	-0.1	3	1016.9	13.0	71	7.9	///	////	111100000
0	50	0.0	3	1016.9	13.4	72	8.5	208	0.5	111100000
0	55	0.1	4	1016.8	13.2	71	8.1	///	////	111100000
1	0	0.0	3	1016.9	12.9	71	7.8	208	0.6	111100000
1	5	0.0	3	1016.9	12.8	72	7.9	. ///	////	111100000
1	10	0.0	3	1016.9	12.9	75	8.6	187	0.5	111100000
1	15	0.1	5	1016.7	13.0	73	8.3	///	////	111100000
1	20	0.1	7	1016.5	12.8	71	7.7	119	0.6	111100000
1	25	0.0	5	1016.7	13.1	72	8.2	///	////	111100000
1	30	0.1	7	1016.5	12.9	70	7.6	139	0.6	111100000
1	35	0.2	8	1016.3	12.8	69	7.3	///	////	111100000
1	40	0.1	7	1016.5	12.8	69	7.3	106	0.7	111100000
1	45	0.1	9	1016.2	12.7	70	7.4	///	////	111100000
1	50	0.1	9	1016.2	12.6	70	7.3	133	0.5	111100000
1	55	0.1	7	1016.5	12.7	70	7.4	///	////	111100000
2	0	0.1	9	1016.2	12.6	71	7.5	99	0.8	111100000
2	5	0.1	9	1016.2	12.7	70	7.4	///	////	111100000
2	10	0.3	15	1015.5	12.6	70	7.3	108	0.8	111100000
2	15	0.3	17	1015.2	12.6	72	7.7	///	////	111100000
2	20	0.2	15	1015.5	12.5	72	7.6	95	1.0	111100000
2	25	0.4	18	1015.1	12.5	71	7.4	///	////	111100000
2	30	0.3	17	1015.2	12.5	72	7.6	98	0.7	111100000
2	35	0.3	19	1015.0	12.6	72	7.7	///	////	111100000
2	40	0.2	21	1014.7	12.3	72	7.5	136	0.5	111100000
2	45	0.3	25	1014.2	12.3	72	7.5	///	////	111100000
2	50	0.6	32	1013.5	12.3	72	7.5	112	0.5	111100000

Start Up Date 22 MAY 95 15:42 GMT System test passed -No errors found Sounding program REV 7.62 using Loran-C

Ship :PT_SUR Location : 36.80 N 121.80 W

Loran-C chain 1: 9940

Phase fitting length is 60 s from 0 min to 10 min Phase fitting length is 120 s from 10 min to 45 min Phase fitting length is 240 s from 45 min to 120 min

Sounding: 31 RS-number: 108234842

No PTU editing No wind editing

Started at: . 22 MAY 95 15:52 GMT

Ti WndSt		AscRate	Hgt/MSL	Pressure	Temp	RH	Dewp	Dir	Speed	
min	s	m/s	m	hPa	degC	%	degC	deg	m/s	
0	0	0.0	3	1015.1	11.2	94	10.3	279	4.1	000000000
0	5	3.7	23	1012.7	12.1	75	7.9	111	////	111100000
0	10	3.7	40	1010.8	11.9	77	8.0	270	4.4	111100000
0	15	3.4	56	1008.8	11.7	79	8.2	111		111100000
0	20	3.3	70	1007.1	11.6	80	8.3	273		111100000
	25	3.2	81	1005.7	11.5	81	8.4	///	////	111100000
	30	3.1	97	1003.9	11.3	82	8.4	277	4.0	111100000
	35	3.1	115	1001.7	11.2	83	8.5	///	////	111100000
	40	3.1	133	999.5	11.0	84	8.4	285		111100000
	45	3.1	149	997.5	10.9	85	8.5	///		111100000
	50	3.3	168	995.3	10.7	86	8.5	276	3.9	111100000
	55	3.5	188	992.9	10.5	85	8.1	///	////	111100000
1	0	3.7	208	990.5	10.3	82	7.4	275	4.0	111100000
1	5	4.0	229	987.9	10.2	83	7.5	///	////	
	10	3.7	245	986.1	10.1	82	7.2	275		111100000
	15	3.6	259	984.5	9.9	83	7.2	///		111100000
	20	3.5	273	982.8	9.7	83	7.0	275	3.6	111100000
	25	3.5	293	980.4	9.6	84	7.1	///	////	111100000
	30	3.4	311	978.2	9.5	81	6.5	289	2.7	111100000
	35	3.2	326	976.6	9.5	81	6.5	///	////	
	40	3.2	340	974.9	9.4	81	6.4	292		111100000
	45	3.1	352	973.5	9.3	81	6.3	111	////	111100000
	50	3.2	370	971.3	9.1	81	6.1	290	2.5	111100000
	55	3.0	381	970.0	9.0	82	6.1	. ///	////	111100000
2	0	2.8		968.5	8.8	82	5.9	281		111100000
2	5	2.7	409		8.7	83	6.0	///		111100000
	10	2.7	422	965.2	8.5	83	5.8	281	2.6	111100000
	15	2.8	434	963.8	8.5	84	6.0	///	////	111100000
2	20	2.6	447	962.4	8.3	85	6.0	290	2.3	111100000

Sounding program REV 7.62 using Loran-C

Ship :PT SUR

Location: 36.80 N 121.80 W 3 m

Loran-C chain 1: 9940

Phase fitting length is 60~s from 0~min to 10~min Phase fitting length is 120~s from 10~min to 45~min Phase fitting length is 240~s from 45~min to 120~min

Sounding: 32 RS-number: 108234754

No PTU editing No wind editing

Started Time WndStat			95 17:57 Pressure	GMT Temp	RH	Dewp	Dir	Speed	
min s	m/s	m	hPa	degC	olo	degC	deg	m/s	•
0 0 0 5 0 10 0 15 0 20 0 25 0 30 0 35 0 40 0 45 0 50 0 55 1 0 1 5 1 10 1 15 1 20 1 25 1 30	0.0 5.8 5.1 5.2 4.6 4.9 4.7 4.6 4.4 5.1 4.5 4.5 4.3 4.5	3 29 54 80 95 123 150 173 192 216 247 264 282 301 326 351 375 397 415	1016.7 1013.5 1010.5 1007.3 1005.6 1002.2 999.0 996.2 993.9 991.1 987.3 985.3 981.0 978.0 975.0 972.3 969.7	degC 11.4 12.6 12.1 11.9 11.7 11.4 11.1 10.9 10.7 10.6 10.4 10.3 10.2 10.2 10.0 9.7 9.5 9.4 9.2	% 89 70 73 74 75 77 79 78 77 76 77 78 79 80 81	degC 9.7 7.5 7.6 7.6 7.1 7.0 6.5 6.2 6.1 6.2 6.2 6.1 6.2	deg 306 /// 313 /// 326 /// 317 /// 332 /// 318 /// 309 /// 298 /// 291	1.6 //// 4.5 //// 4.2 //// 4.0 //// 3.8 //// 3.6 //// 3.5 ////	000000000 110100000 110100000 110100000 110100000 110100000 110100000 110100000 110100000 110100000 110100000 110100000 110100000 110100000 110100000 110100000 110100000 110100000
1 35 1 40 1 45 1 50	4.6 4.7 4.9 4.6	436 467 496 512	965.1 961.4 958.1 956.3	9.0 8.7 8.5 8.3	82 84 86 87	6.1 6.2 6.3 6.3	///· 277 /// 285		110100000 110100000 111100000 111100000
1 55 2 0 2 5 2 10 2 15	4.4 4.5 4.5 4.2 3.7	532 550 572 592	953.9 951.8 949.3 947.0	8.1 8.0 7.8 7.7	88 89 90 90	6.3 6.3 6.2	/// 281 /// 274	//// 1.8 //// 1.9	111100000
2 20 2 25 2 30 2 35 2 40	3.8 3.9 3.9 3.9 3.8	607 626 650 668 687 706	945.2 943.1 940.3 938.2 936.1 933.9	7.6 7.5 7.4 7.3 7.2 7.1	91 91 91 91 91	6.3 6.2 6.1 6.0 5.9	/// 261 /// 257 /// 249	//// 2.4	111100000 111100000 111100000 111100000
2 45	3.9	726	931.6	7.0	92	5.8	///	////	111100000

May 23	1600							
0 5	4.5	23	1011.5	12.9	69	7.4	///	////CD-FGH
0 10	4.7	50	1008.3	12.2	72	7.4	263	2.6CD-FGH
0 15	4.6	71	1005.7	12.0	74	7.6	///	////CD-FGH
0 20	4.6	95	1002.9	11.7	75	7.5	228	2.3 CD-FGH
0 25	4.5	115	1000.4	11.6	76	7.6	///	////CD-FGH
0 30	4.4	136	998.0	11.3	77	7.5	226	2.3 CD-FGH
0 35	4.3	153	995.9	11.2	78	7.6	///	////CD-FGH
0 40	4.0	170	993.9	11.0	.78	7.4	234	2.2 CD-FGH
0 45	4.0	191	991.3	10.8	79	7.4	111	////CD-FGH
0 50	3.8	209	989.3	10.6	80	7.3	231	2.2 CD-FGH
0 55	3.9	230	986.7	10.4	81	7.3	///	//// -BCD-FGH
1 0	3.7	247	984.7	10.2	81	7.1	222	2.2 -BCD-FGH
1 5	4.3	276	981.2	10.0	83	7.3	///	//// -BCD-FGH
1 10	4.3	298	978.7	9.7	84	7.2	230	2.0 -BCD-FGH
1 15	4.1	315	976.7	9.6	86	7.4	///	//// -BCD-FGH
1 20	4.0	330	974.9	9.5	86	7.3	214	2.1 -BCD-FGH
1 25	3.8	350	972.5	9.4	87	7.4	///	//// -BCD-FGH
1 30	3.8	362	971.1	9.2	87	7.2	226	1.8 -BCD-FGH
1 35	3.9	394	967.4	9.1	87	7.1	///	
1 40 1 45	3.8	413	965.2	9.0	87	7.0	228	1.6 -BCD-FGH
1 50	4.0 4.2	436 457	962.5 960.0	8.9	88	7.1	///	//// -BCD-FGH
1 55	4.4	471	958.4	8.8	88	7.0	233	1.5 -BCD-FGH
2 0	4.5	497	955.3	8.7 8.6	88	6.9	///	//// -BCD-FGH
2 5	4.0	517	953.1	8.5	88 88	6.8 6.7	240	1.3 -BCD-FGH
2 10	4.5	548	949.5	8.4	88	6.6	/// 253	//// -BCD-FGH
2 15	4.4	567	947.3	8.3	88	6.5	///	1.1 -BCD-FGH
2 20	4.6	594	944.2	8.1	88	6.3	259	1.0 -BCD-FGH
2 25	4.3	612	942.1	8.1	88	6.3	///	//// -BCD-FGH
2 30	4.7	638	939.1	7.9	87	5.9	273	0.8 -BCD-FGH
2 35	4.3	647	938.1	7.9	87	5.9	///	//// -BCD-FGH
2 40	4.3	678	934.6	8.3	89	6.6	303	0.8 -BCD-FGH
2 45	4.7	708	931.3	9.8	90	8.3	111	//// -BCD-FGH
2 50	4.2	721	929.8	10.5	90	9.0	331	1.1 -BCD-FGH
2 55	4.2	737	928.0	10.8	90	9.3	///	//// -BCD-FGH
3 0	3.9	755	925.9	10.8	87	8.8	345	1.5 -BCD-FGH
3 5	4.2	772	924.0	10.8	85	8.4	///	//// -BCD-FGH
3 10	3.6	786	922.6	11.1	85	8.7	350	1.9 -BCD-FGH
3 15 3 20	3.6	811	919.7	11.6	84	9.0	///	//// -BCD-FGH
3 25	3.8 3.8	835 847	917.2 915.8	12.1	82	9.2	356	2.6 -BCD-FGH
3 30	3.6	863	913.0	12.2 12.3	80 79	8.9		//// -BCD-FGH
3 35	3.7	883	911.8	12.3	80	8.8 9.0	6 ///	2.9 -BCD-FGH //// -BCD-FGH
3 40	3.7	896	910.5	12.5	81	9.4	6	3.5 -BCD-FGH
3 45	3.4	914	908.5	12.7	81	9.6	///	//// -BCD-FGH
3 50	3.3	933	906.5	12.8	80	9.5	6	4.0 -BCD-FGH
3 55	3.5	953	904.3	13.0	80	9.7	///	//// -BCD-FGH
4 0	3.9	980	901.4	13.0	81	9.9	5	4.4 -BCD-FGH
4 5	3.4	991	900.2	12.9	80	9.6	111	//// -BCD-FGH
4 10	3.7	1008	898.3	12.8	79	9.3	360	5.5 -BCD-FGH
4 15	4.0	1040	894.9	13.1	79	9.6	///	//// -BCD-FGH
4 20	4.7	1074	891.3	13.0	80	9.7	359	6.1 -BCD-FGH
4 25	4.5	1091	889.5	13.0	79	9.5	///	//// -BCD-FGH
4 30	4.0	1100	888.5	13.1	74	8.6	358	6.8 -BCD-FGH
4 35 4 40	4.5	1121	886.3	13.1	72	8.2	///	//// -BCD-FGH
4 40	4.4	1141	884.2	13.3	72	8.4	357	7.1 -BCD-FGH

Sounding program REV 7.62 using Loran-C
Ship :PT_SUR
Location: 36.80 N 121.80 W 3 m
Loran-C chain 1: 9940
Phase fitting length is 60 s from 0 min to 10 min
Phase fitting length is 120 s from 10 min to 45 min
Phase fitting length is 240 s from 45 min to 120 min
Sounding: 35

RS-number: 108234749

No PTU editing No wind editing

Start Up Date 23 MAY 95 16:57 GMT System test passed -No errors found Sounding program REV 7.62 using Loran-C

Ship :PT SUR

Location: 36.80 N 121.80 W 3 m

Loran-C chain 1: 9940

Phase fitting length is 60 s from 0 min to 10 min Phase fitting length is 120 s from 10 min to 45 min Phase fitting length is 240 s from 45 min to 120 min

Sounding: 35 RS-number: 108234749

No PTU editing

Started manually by operator

Started at: 23 MAY 95 17:05 GMT

Time WndStat	AscRate	Hgt/MSL	Pressure	Temp	RH	Dewp	Dir	Speed	
min s	m/s	m	hPa	degC	8	degC	deg	m/s	·
0 0	0.0	3	1015.0	12.7	76	8.6	184	0.7	000000000
0 5	-0.7	-1	1015.5	12.8	77	8.9	134	2.6	111100000
0 10	-0.6	-3	1015.7	12.7	78	9.0	109	3.6	111100000
0 15	-0.3	-2	1015.6	12.8	79	9.3	97	3.9	111100000
. 0 20	-0.2	-1	1015.5	12.7	78	9.0	86	3.9	111100000
0 25	-0.1	2	1015.1	12.8	78	9.1	82	3.6	111100000
0 30	-0.1	1	1015.2	12.7	78	9.0	82	3.2	111100000
0 35	0.1	2	1015.1	12.7	78	9.0	85	2.9	111100000
0 40	0.1	1	1015.2	12.6	78	8.9	90	2.4	111100000
0 45	0.1	2	1015.1	12.7	79	9.2	95	2.1	111100000
0 50	0.1	1	1015.2	12.7	78	9.0	100	1.7	111100000
0 55	0.0	2	1015.1	12.7	79	9.2	100	1.8	111100000
1 0	0.1	3	1015.0	13.1	79	9.6	101	1.6	111100000
1 5	0.1		1014.6	13.2	78	9.5	103	1.5	111100000
1 10	0.2	7	1014.5	13.3	77	9.4	103	1.4	111100000
1 15	0.1	8	1014.3	13.5	77	9.6	103	1.3	111100000
1 20	0.1	5	1014.7	14.0	76	9.9	101	1.2	111100000
1 25	0.2	7	1014.5	13.6	76	9.5	99	1.1	111100000
1 30	0.2	9	1014.2	13.0	75	8.7	96	1.0	111100000
1 35	0.3	12	1013.8	12.6	77	8.7	95	1.0	111100000
1 40	0.1	11	1014.0	12.5	77	8.6	94	1.0	111100000
1 45	0.3	14	1013.6	12.4	79	8.9	93	1.0	111100000
1 50	0.3	15	1013.5	12.4	81	9.3	93	0.9	111100000
1 55	0.2	13	1013.7	12.3	81	9.2	93	0.9	111100000
2 0	0.1		1013.7	12.2	80	8.9	93	0.9	111100000
2 5	-0.1	12	1013.8	12.3	81	9.2	93	0.9	111100000
2 10	0.0	11	1014.0	12.3	81	9.2	94	0.9	111100000

Sounding program REV 7.62 using Loran-C

Ship :PT_SUR

Location: 36.80 N 121.86 W

Loran-C chain 1: 9940

Phase fitting length is 60 s from 0 min to 10 min Phase fitting length is 120 s from 10 min to 45 min Phase fitting length is 240 s from 45 min to 120 min

Sounding: 36 RS-number: 108234749

No PTU editing

Started manually by operator Started at: 23 MAY 95 19:16 GMT

T: WndSt		AscRate	Hgt/MSL	Pressure	Temp	RH	Dewp	Dir	Speed	
min	s	m/s	m	hPa	degC	ે	degC	deg	m/s	
0	0	0.0	3	1015.8	12.6	86	10.3	269	2 0	00000000
0	5	0.0	2	1015.8	12.6	85	10.3	243		
0	10	0.0	3	1015.7	12.6	84	10.2		2.0	
0	15	0.0	4	1015.7	12.6	84	10.0	219 215	1.4	
0	20	0.0	3	1015.7	12.6	84	10.0	199	1.1	
0	25	-0.1	1	1016.0	12.5	84	9.9			111100000
0	30	-0.1	1	1016.0	12.8	84	10.2	165		111100000
0	35	-0.1	-1	1016.0	12.4	85	10.2	116 109	0.5 0.5	111100000 111100000
0	40	-0.1	-1	1016.2	12.4	85	10.0	112	0.5	111100000
0	45	0.1	4	1015.6	12.4	85	10.4	103	0.5	
0	50	0.1	7	1015.0	12.6	85	10.4	78		111100000 111100000
0	55	0.1	8	1015.2	12.8	84	10.2	68	0.8	
1	0	0.1	5	1015.5	12.6	84	10.2	56		111100000
1	5	0.3	5 6	1015.3	12.5	85	10.0	42	0.5	
1	10	0.2	5	1015.5	12.4	84	9.8	0	0.0	111100000
1	15	-0.1	5 5	1015.5	12.5	85	10.1	0	0.0	
1	20	0.1	9	1015.0	12.6	85	10.1	0	0.0	
1	25	0.1	12	1013.6	12.4	84	9.8	0		111100000
1	30	0.4	17	1014.0	12.1	85	9.7	0		111100000
1	35	0.5	22	1013.4	12.0	85	9.6	0		111100000
1	40	0.7	25	1013.4	12.0	8.5	9.6	0		111100000
1	45	1.0	35	1011.9	11.9	86	9.7	Ö		111100000
1	50	1.0	40	1011.3	11.8	86	9.6	328		111100000
1	55.	1.2	46	1010.5	11.8	86	9.6	332	0.5	
2	0	1.2	54	1009.5	11.7	86	9.5	332		111100000
2	5	1.3	60	1008.8	11.7	87	9.7	326	0.5	
2	10	1.3	64	1008.3	11.6	87	9.6	320	0.5	
2	15	1.3	73	1007.2	11.5	87	9.5	314	0.5	111100000
2	20	1.2	76	1006.8	11.5	87	9.5	0	0.0	
2	25	1.1	81	1006.2	11.4	88	9.5	Ö	0.0	
2	30	0.9	82	1006.1	11.4	88	9.5	0		111100000
2	35	1.0	89	1005.3	11.3	88	9.4	0	0.0	
2	40	1.0	95	1004.6	11.3	88	9.4	Ö	0.0	111100000
2	45	1.0	103	1003.6	11.2	88	9.3	Ô		111100000
_					· -		J. J	Ü	0.0	111100000

Sounding program REV 7.62 using Omega Ship :PT_SUR
Location: 36.77 N 121.90 W 3 m
Rejected Sigma stations: a,b,c

Phase fitting length is 250 s from 0 min to 120 min

Sounding: 37 RS-number: 309140455

No PTU editing No wind editing

Started at: 23 MAY 95 21:06 GMT

Time WndStat	AscRate	Hgt/MSL	Pressure	Temp	RH	Dewp	Dir	Speed
min s	m/s	m	hPa	degC	엉	degC	deg	m/s
0 0	0.0	3	104.3	11.9	93	10.8	236	1.9
0 5	-461.8	14/1//	1011.4	12.9	76	8.8	///	////CDGH
0 10	-277.1	//////	1009.0	12.3	80	9.0	190	2.3CDGH
0 15	-173.2	//////	1005.6	12.0	83	9.3	///	////CDGH
0 20	-138.6	//////	1003.0	11.8	84	9.2	201	1.9CDGH
0 25	-106.6	//////	998.9	11.6	85	9.2	///	////CDGH
0 30	-92.4	//////	997.0	11.4	86	9.2	244	1.5CDGH
0 35	0.0	//////	994.8	11.2	87	9.2	///	////CD-FGH
0 40	0.0	//////	992.7	11.0	88	9.1	249	1.6CD-FGH
0 45	0.0	//////	991.2	10.9	89	9.2	///	////CD-FGH
0 50	0.0	//////	989.5	10.7	89	9.0	285	2.2 CD-FGH
0 55	0.0	//////	987.0	10.6	90	9.1	///	////CD-FGH
1 0	0.0	//////	984.5	10.4	91	9.0	260	1.6CD-FGH
1 5	0.0	//////	983.3	10.3	92	9.1	///	////CD-FGH
1 10	0.0	//////	981.1	10.1	93	9.1	257	1.5CD-FGH
1 15	0.0	11/1//	979.1	10.0	94	9.1	111	////CD-FGH
. 1 20	0.0	111111	977.0	9.9	95	9.2	255	1.6CD-FGH
1 25	0.0	111111	974.3	9.7	96	9.1	111	////CD-FGH
1 30	0.0	//////	970.6	9.6	96	9.0	296	2.6CD-FGH
1 35	0.0	11/1//	967.8	9.5	96	8.9	111	////CD-FGH
1 40	0.0	//////	964.7	9.3	97	8.9	304	3.1CD-FGH
1 45	0.0	//////	962.7	9.2	96	8.6	111	////CD-FGH
1 50	0.0	//////	959.1	9.0	96	8.4	311	3.9CD-FGH
1 55	0.0	//////	956.4	9.0	97	8.6	111	////CD-FGH
2 0	0.0	//////	953.7	8.8	97	8.4	311	3.9CD-FGH
2 5	0.0	//////	950.3	8.7	97	8.3	///	////CD-FGH
2 10	0.0	//////	946.7	9.1	98	8.8	314	4.1CD-FGH
2 15	0.0	//////	944.2	10.0	99	9.9	///	//// CD-FGH
2 20	0.0	//////	942.1	10.3	98	10.0	316	4.6CD-FGH
2 25	0.0	//////	940.3	10.5	94	9.6	///	////CD-FGH
2 30	0.0	//////	938.5	10.6	92	9.4	319	5.0CD-FGH
2 35	0.0	//////	936.2	11.2	95	10.5	111	////CD-FGH
2 40	0.0	/////	933.4	12.5	95	11.8	319	4.8CD-FGH
2 45	0.0	//////	932.0	13.0	93	11.9	///	////CD-FGH
2 50	0.0	/////	930.0	13.2	91	11.8	322	5.6CD-FGH
2 55	0.0	//////	927.4	13.3	88	11.4	///	////CD-FGH

APPENDIX J. MATLAB CODE FOR COMPUTATION

A. GPS, ELEVATION AND AZIMUTH ANGLE CALCULATION

```
% GPS & elevation & azimuth angle caculation
% File name gps.m
ship_longitude=121.81;
ship latitude=36.81;
sensor_longitude=121.8;
sensor latitude=36.8;
heading=120;
dx=(ship_longitude-sensor_longitude)*47.995;
dy=(ship latitude-sensor latitude)*59.97;
a=(atan(abs(dx/dy)))*57.3
if dy>0
  if heading>(180-a)
   bearing=(heading-180+a);
  else
    bearing=180-a-heading
  end
else
  if heading<a
   bearing=a-heading;
   bearing=heading-a;
  end
end
if bearing<90
  phi=(90-bearing)/57.3
else
  phi=(180-bearing)/57.3
end
range in nmi=sqrt(dx*dx+dy*dy)
range_in_km=(range_in_nmi)*1.852
```

theta=atan(0.0032/range_in_nmi)

l=41.5; %sh w=9.75; %sh

%ship length %ship width

h=8.8;

%ship height

Area=l*w*sin(theta)+h*w*cos(theta)*sin(phi)+h*l*cos(theta)*cos(phi)

B. MRT &MDT vs Spatial Frequency

```
% MRT & MDT vs Spatial Frequency
 % File name drt fre
                                                                        % Shumaker Example 8-13
 SNRT=2.5;
NET=0.125;
dx=0.25;
 dy=0.25;
L=7;
Te=0.1;
Fr=30;
Nos=1;
Nss=1;
rb=0.335;
rs=0.456;
v=0.000001:0.25:3.000001;
MTF=[1 0.89 0.79 0.64 0.53 0.43 0.35 0.27 0.2 0.15 0.1 0.07 0.04];
omigaT=1./(4*v.*v);
ROx=(1+(2*2*v.*v*rb.*rb)).^(-0.5);
MRT = 2*SNRT*NET*(ROx.^0.5).*((v.*v*dx*dy/L).^0.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.
0.5)./MTF;
MDT_1=SNRT*NET*(omigaT+rs*rs)*((dx*dy)^0.5);
 MDT_2 = omigaT.*((((pi/4)*(rs*rs+rb*rb+omigaT)*Te*Fr*Nos*Nss)).^0.5);
MDT=MDT 1./MDT 2;
plot(v,MDT,v,MRT);
title('MRT & MDT vs Spatial Frequency');
xlabel('Spatial Frequency');
ylabel('Temperature');
gtext('MRT');
gtext('MDT');
grid;
```

C. MRT, MDT & ΔT vs Range for Detection

```
% MRT & MDT vs & Range
% N=1 for Detection
% File name r n 1 f
SNRT=2.5;
                        % Shumaker Example 8-13
NET=0.125;
dx=0.25;
dy=0.25;
L=7;
Te=0.1:
Fr=30;
Nos=1;
Nss=1:
rb=0.335;
rs=0.456;
N=1;
                     % physical dimension
At=214.4513;
Dc=(At)^{(0.5)};
X=Dc/N;
dt=3.387144;
u=0.0002132;
v=0.000001:0.25:3.000001;
MTF=[1 0.89 0.79 0.64 0.53 0.43 0.35 0.27 0.2 0.15 0.1 0.07 0.04];
Range=v*2000*X;
omigaT=1./(4*v.*v);
ROx=(1+(2*2*v.*v*rb.*rb)).^(-0.5);
tau=exp(-u.*Range);
dtapp=dt*tau;
MRT=2*SNRT*NET*(ROx.^0.5).*((v.*v*dx*dy/L).^0.5).*((Te*Fr*Nos*Nss)^(-
0.5))./MTF;
MDT_1=SNRT*NET*(omigaT+rs*rs)*((dx*dy)^0.5);
MDT 2=omigaT.*(((pi/4)*(rs*rs+rb*rb+omigaT)*Te*Fr*Nos*Nss)).^0.5);
MDT=MDT 1./MDT 2;
```

```
plot(Range,MDT,Range,MRT,Range,dtapp);
title('MRT, MDT & dT vs Range for Detection');
xlabel('Range (m)');
ylabel('Temperature');
gtext('MRT');
gtext('MDT');
grid;
```

D. MRT & ΔT vs Range for Classification

```
% MRT & dt vs Range
  % N=8 for Classification
  % File name r n 8 f
  SNRT=2.5;
                                                                                                % Shumaker Example 8-13
 NET=0.125;
  dx=0.25;
  dy=0.25;
  L=7;
 Te=0.1;
 Fr=30;
 Nos=1;
 Nss=1;
 rb=0.335;
 rs=0.456;
 N=8;
                                                                                   % physical dimension
 At=214.4513;
 Dc=(At)^{(0.5)};
 X=Dc/N;
 dt=3.387144;
 u=0.0002132;
 v=0.000001:0.25:3.000001;
 MTF=[1 0.89 0.79 0.64 0.53 0.43 0.35 0.27 0.2 0.15 0.1 0.07 0.04];
 Range=v*2000*X;
 omigaT=1./(4*v.*v);
ROx=(1+(2*2*v.*v*rb.*rb)).^(-0.5);
tau=exp(-u.*Range);
 dtapp=dt*tau;
MRT=2*SNRT*NET*(ROx.^0.5).*((v.*v*dx*dy/L).^0.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)
0.5))./MTF;
MDT_1=SNRT*NET*(omigaT+rs*rs)*((dx*dy)^0.5);
MDT_2=omigaT.*(( ((pi/4)*(rs*rs+rb*rb+omigaT)*Te*Fr*Nos*Nss)).^0.5);
MDT=MDT 1./MDT 2;
```

```
plot(Range,MRT,Range,dtapp);
title('MRT & dT vs Range for Classification');
xlabel('Range (m)');
ylabel('Temperature');
gtext('MRT');
grid;
```

E. MRTD AND ΔT VS RANGE FOR IDENTIFICATION

```
% MRT & dT vs Range
  % N=12.8 for Identification
 % File name r_n_128_f
  SNRT=2.5;
                                                                                               % Shumaker Example 8-13
 NET=0.125;
 dx=0.25;
 dy=0.25;
 L=7;
 Te=0.1;
Fr=30;
Nos=1;
Nss=1;
rb=0.335;
rs=0.456;
N=12.8;
                                                                                              % physical dimension
At=214.4513;
Dc=(At)^{(0.5)};
X=Dc/N;
dt=3.387144;
u=0.0002132
v=0.000001:0.25:3.000001;
MTF=[1 0.89 0.79 0.64 0.53 0.43 0.35 0.27 0.2 0.15 0.1 0.07 0.04];
Range=v*2000*X:
omigaT=1./(4*v.*v);
ROx=(1+(2*2*v.*v*rb.*rb)).^(-0.5);
tau=exp(-u.*Range);
dtapp=dt*tau;
MRT = 2*SNRT*NET*(ROx.^0.5).*((v.*v*dx*dy/L).^0.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.5)).*((Te*Fr*Nos*Nss)^(-1.
0.5))./MTF;
MDT_1=SNRT*NET*(omigaT+rs*rs)*((dx*dy)^0.5);
MDT_2 = omigaT.*((((pi/4)*(rs*rs+rb*rb+omigaT)*Te*Fr*Nos*Nss)).^0.5);
MDT=MDT 1./MDT 2;
```

```
plot(Range,MRT,Range,dtapp);
title('MRT & dT vs Range for Identification');
xlabel('Range (m)');
ylabel('Temperature');
gtext('MRT');
grid;
```

LIST OF REFERENCES

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- Zeisse C.R., SeaRad, A Sea Radiance Prediction Code, Technical Report 1702, Naval Command, Control and Ocean Surveillance Center, RDT and E Division, November 1995.
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